



Great Designs in

STEEL

Fracture Characterization of Advanced 980 MPa Steels

- collaborative project between Steel Marketing Development Institute, Honda Research America, and University of Waterloo

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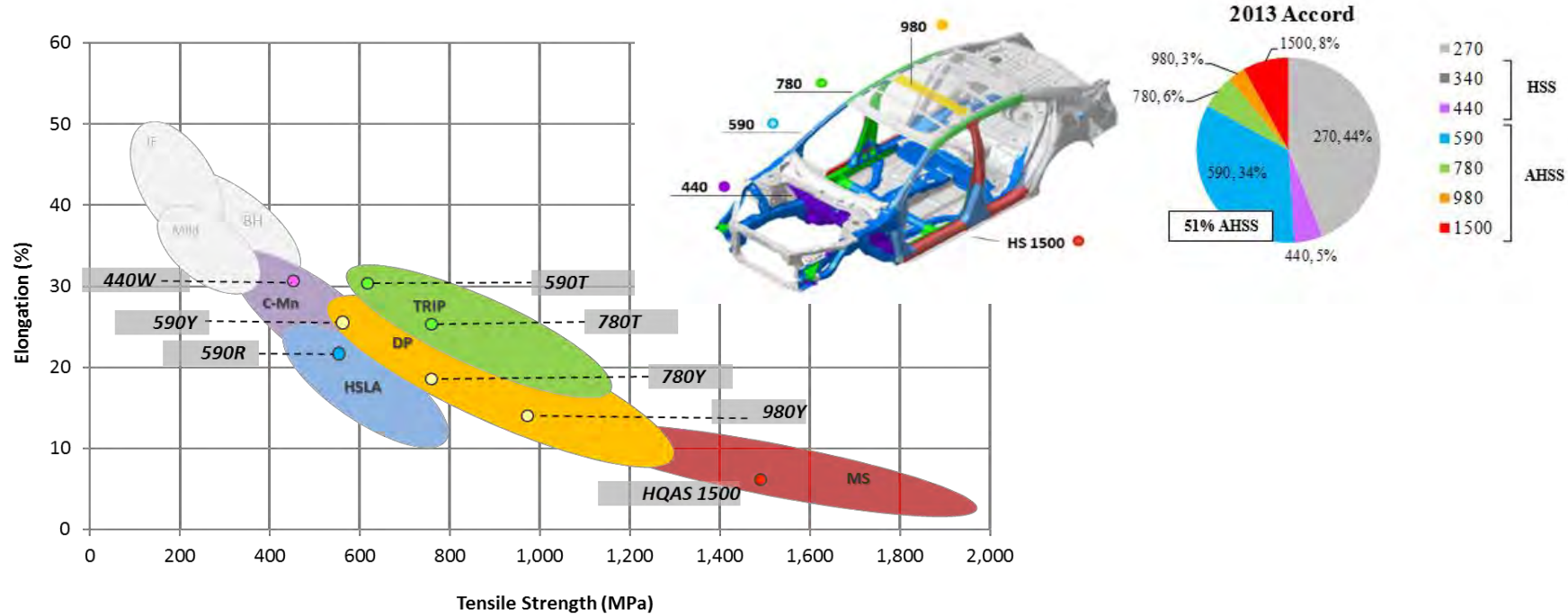
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- **Background**
- **Objective**
- **Study Materials**
- **Fracture Test Methodology and Results**
- **Component Testing**
- **Conclusions**

Background

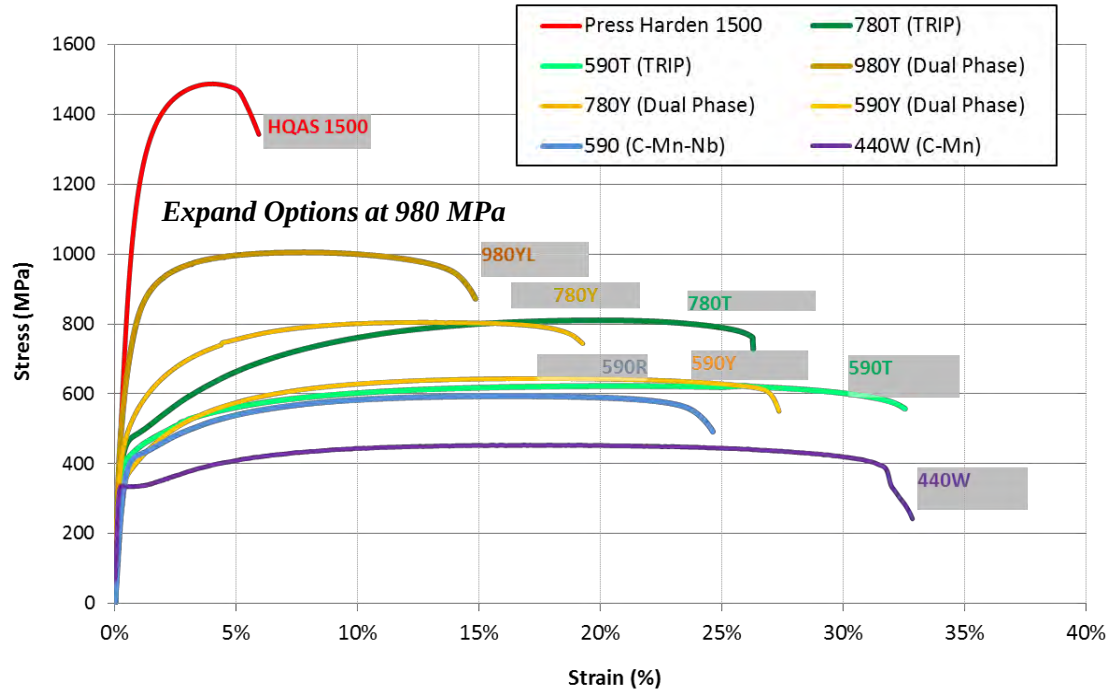
Recent evolution of Advanced High Strength Steel



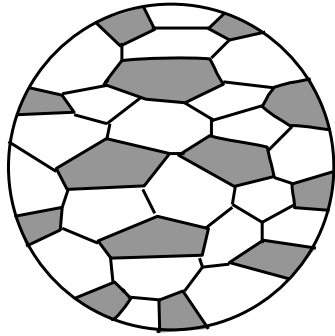
Common AHSS grades and their application areas

Need for Grade Diversification at 980 Strength Level

- Specialized grades now exist at the 590 and 780 MPa strength level. (dual phase, TRIP, etc).
- Expand Grades at 980 MPa for enhanced:
 - bending
 - flanging
 - energy absorption

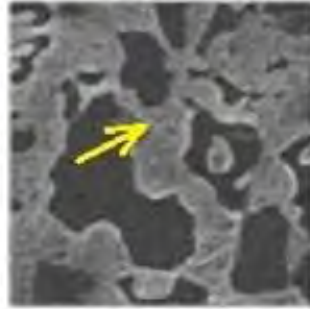


Background

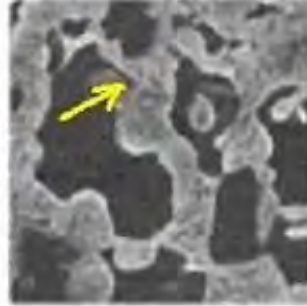


CONV 980YL

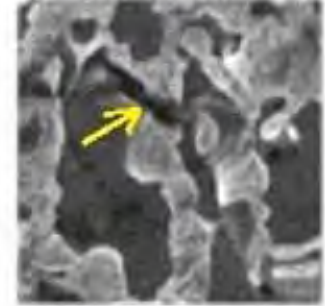
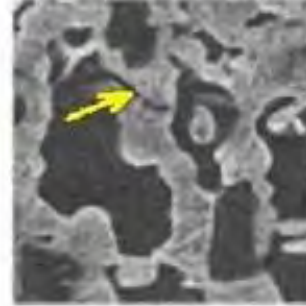
**Initial
Microstructure***



Fracture of martensite



Void Growth



*Damage in dual phase steel DP1000 (Alharbi, K)

- Increasing Strain -

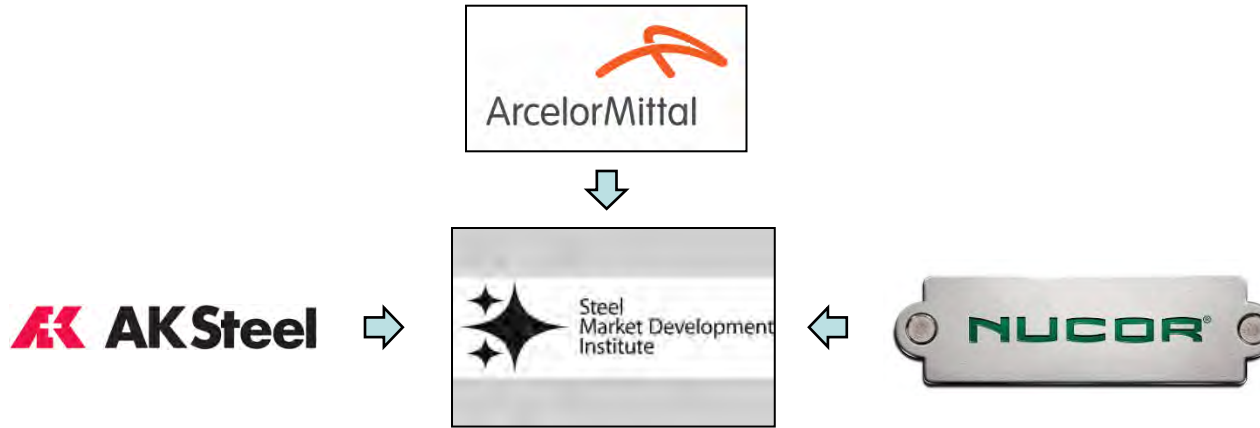
- Microstructures of early DP980 not optimized for bending and edge stretch
- These property limitations restricted the application of DP980.
 - ↳ Complex part shapes and features could not be formed.
 - ↳ Energy absorption targets could not be met due to fracture problems.

Objectives

1. Characterize properties of various Dual Phase 980 grades selected by Steel Marketing Development Institute (*Blind Study*)
2. Investigate optimized fracture testing methodology for Advanced High Strength Steel → ***Industrial Friendly and Efficient Methods Required***
3. Perform experimental axial and bend crush experiments and assess fracture performance

Project Structure

1. Each Supplier Submits One DP980 to SMDI Sample Bank



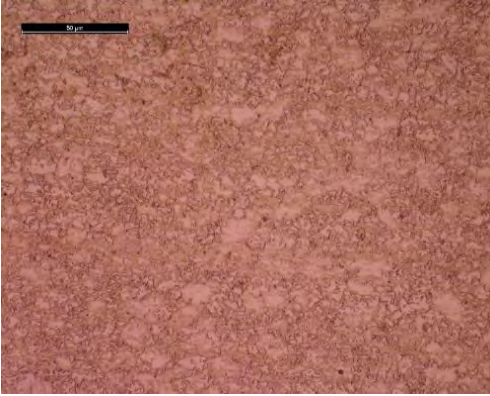
2. Material identification removed:

Sent to UW and Honda for Fracture Characterization from Coupons to Crash

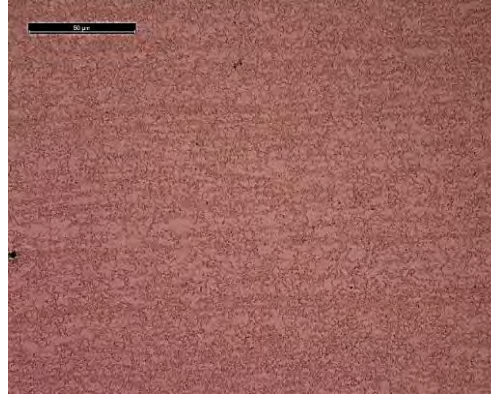


Study Materials: Composition

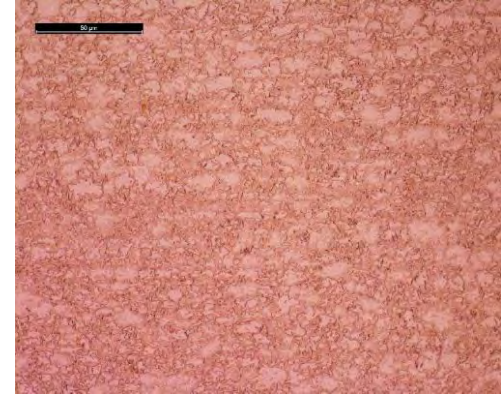
980 #1



980 #2



980 #3

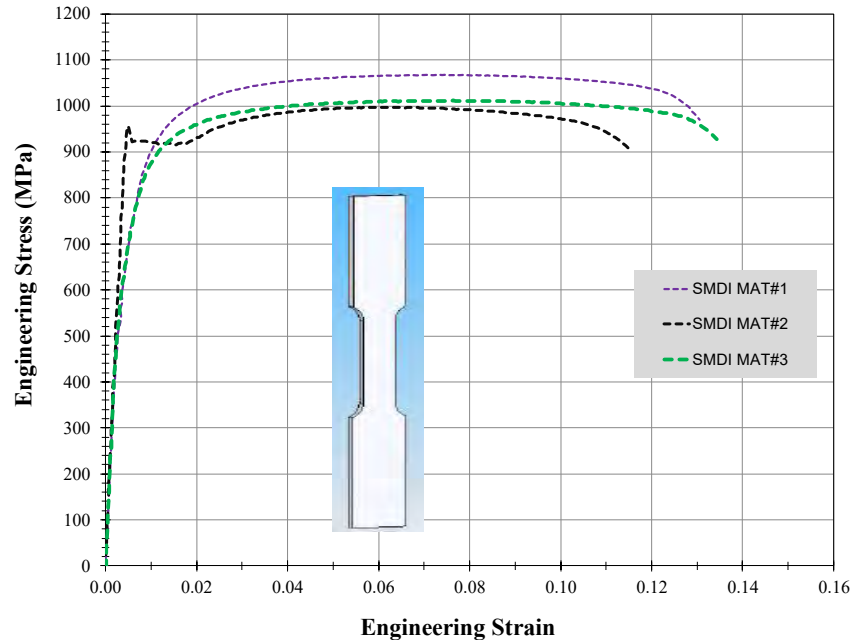


SMDI Grades	Thickness (mm)	Type	General Composition	Coating
980 Mat#1	1.2	Dual Phase	C-Mn-Si	Bare
980 Mat#1	1.6	Dual Phase	C-Mn-Cr-Mo-Nb	Zinc
980 Mat#3	1.4	Dual Phase	C-Mn-Si	Zinc

Materials can generally be described as DP with fine, uniform microstructure.

Grades represent recent optimization in processing / chemistry (*but are not Gen 3 level*)

Study Materials: Tensile Properties

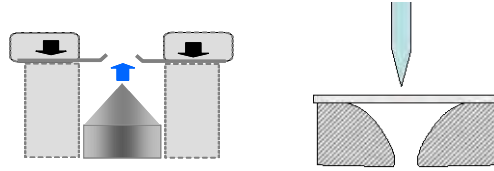


Tensile Properties - JIS Test Specimen

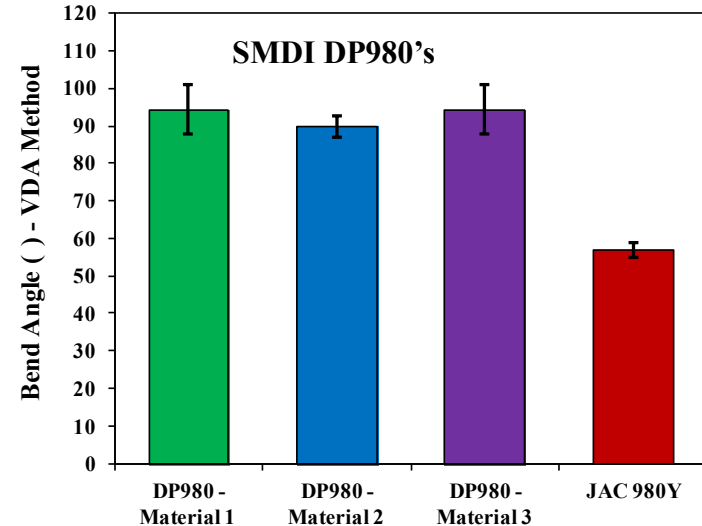
Grade		TS (MPa)	YS (MPa)	YS/TS Ratio	TE (%)
#1	L	1046	806	0.81	12.7
	T	1067	787	0.74	13.5
#2	L	971	912	0.94	12.9
	T	998	934	0.94	12.0
#3	L	989	776	0.78	13.8
	T	1012	757	0.75	13.0

- All grades exhibited total elongation typical of 980 level material.
- Relatively high YS/TS ratios suggested all grades favor local formability.
- Material #2 had unique yield point elongation behavior.

Local Ductility Properties - Hole Expansion and Bendability



Grade		Hole Expansion (punched) (%)	Bend (VDA Angle)
#1	L	36	105°
	T		95°
#2	L	44	102°
	T		90°
#3	L	39	110°
	T		95°



- Performance of these grades is consistent with or above current commercial products.
- VDA bend data is of growing industrial importance as means to evaluate material.
- ➔ *The potential use of the VDA test for fracture prediction will be elaborated on in next section*

Characterization for Formability & Fracture

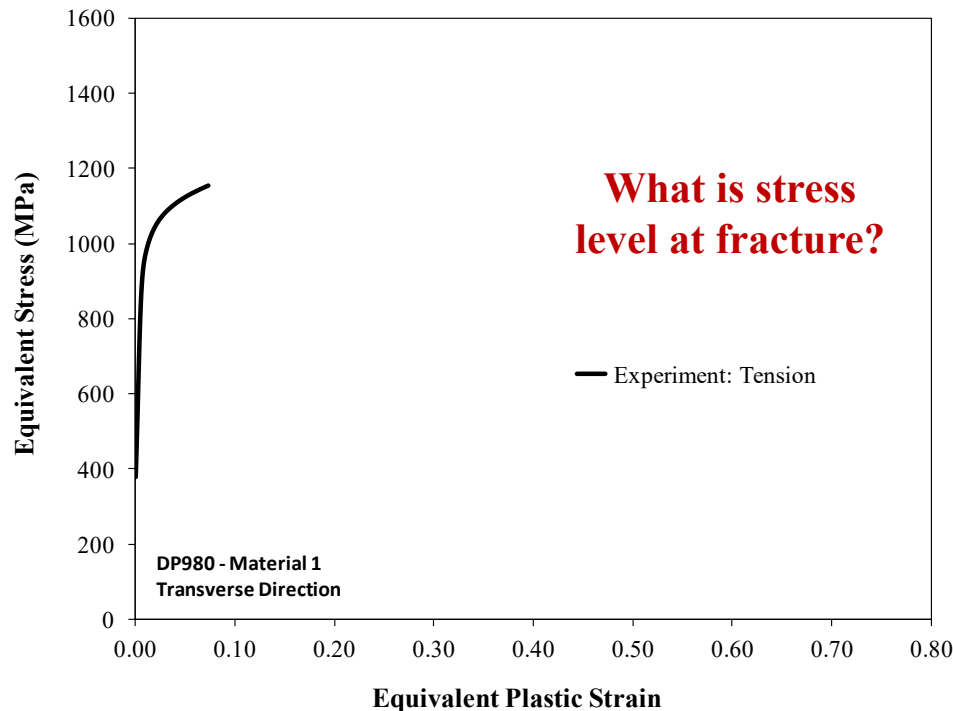
Priority Focus Areas

- 1) Material characterization at large strains and strain rates
- 2) Efficient method to determine forming limit strains (FLD) (*Global formability*)
- 3) Characterization in tight radius bending (*Local formability/fracture*)
- 4) Establish best practices and tests for experimental fracture characterization

*Extensive numerical characterization study pursued in tandem

1. Material Characterization at Large Strains

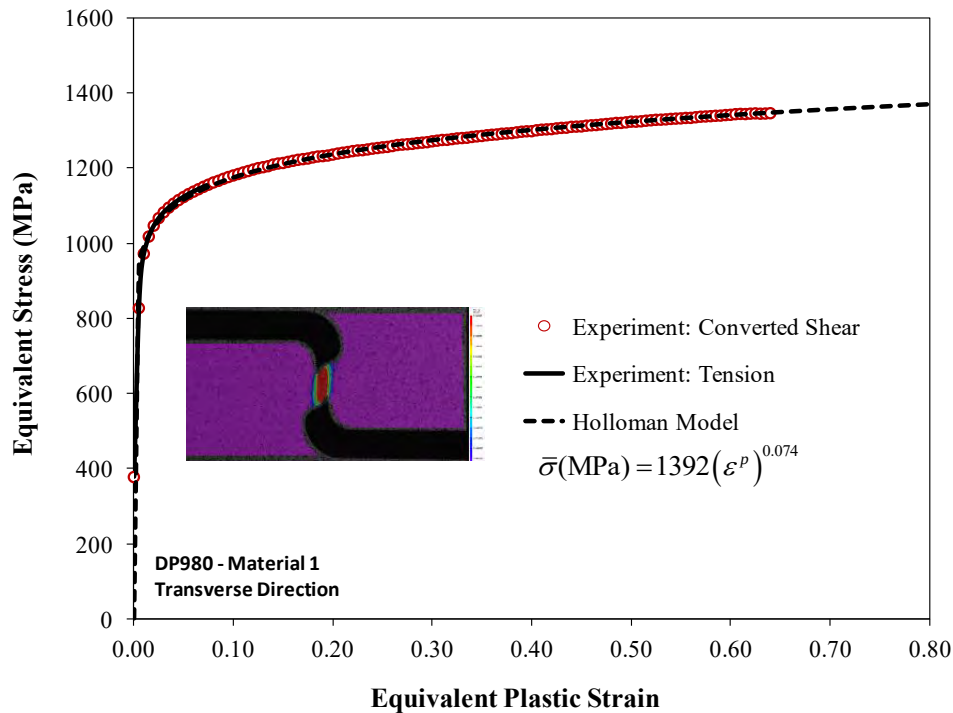
- Limited hardening data available in tensile tests
- Inverse FE modeling used to identify hardening at large strains for fracture
- Hardening data becomes a function of numerical model assumptions...



1. Material Characterization at Large Strains

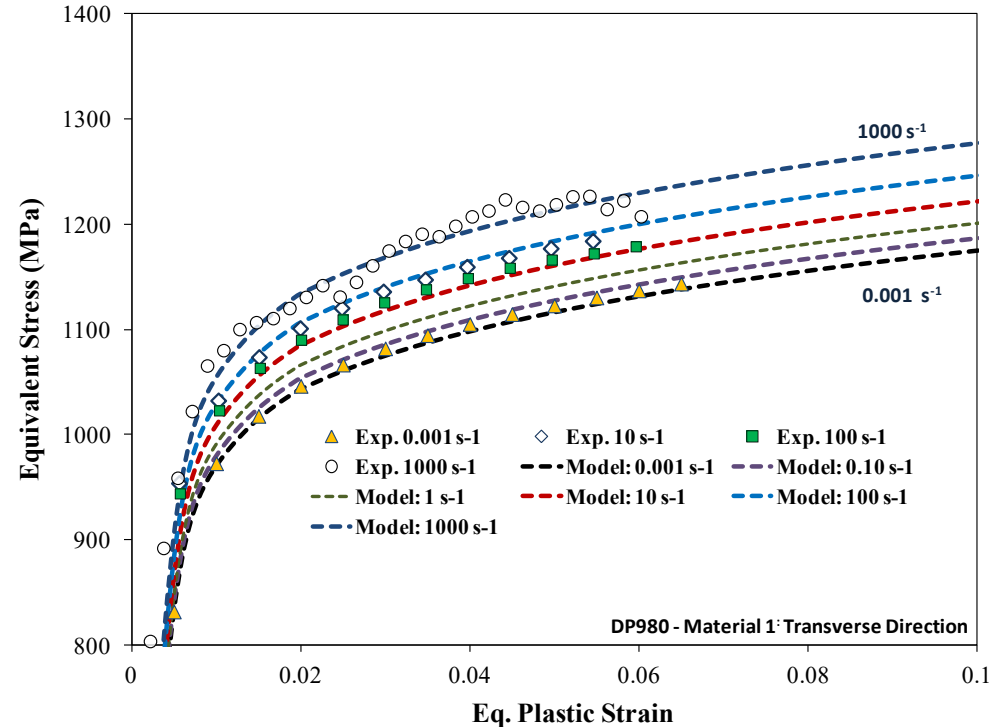
- UW developed simple method to use tensile & shear test data to obtain hardening to large strain levels
- DP980 data to 60% strain!
- Not related to FE model

Methodology in Rahman, T., et al.,
Int. J. Impact. Eng., 2017 (in-press)



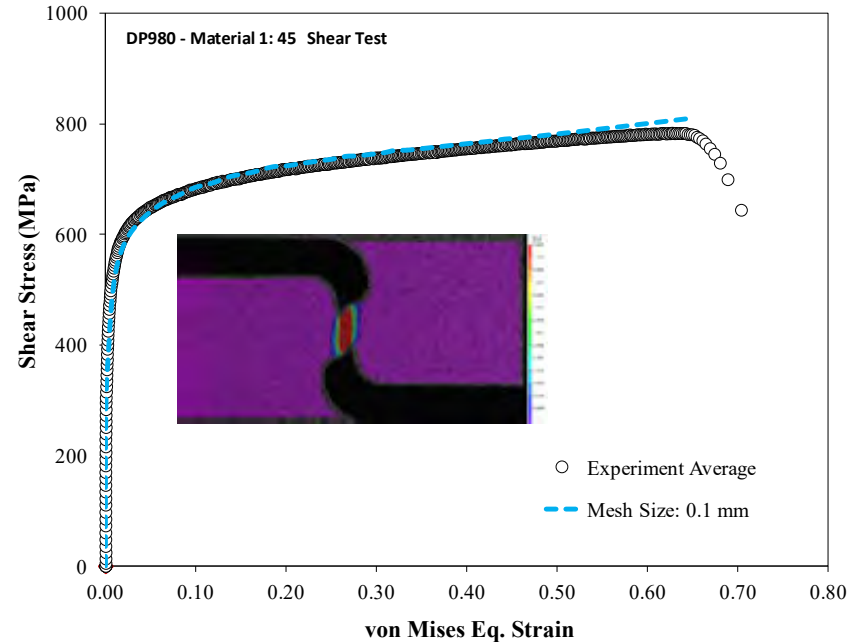
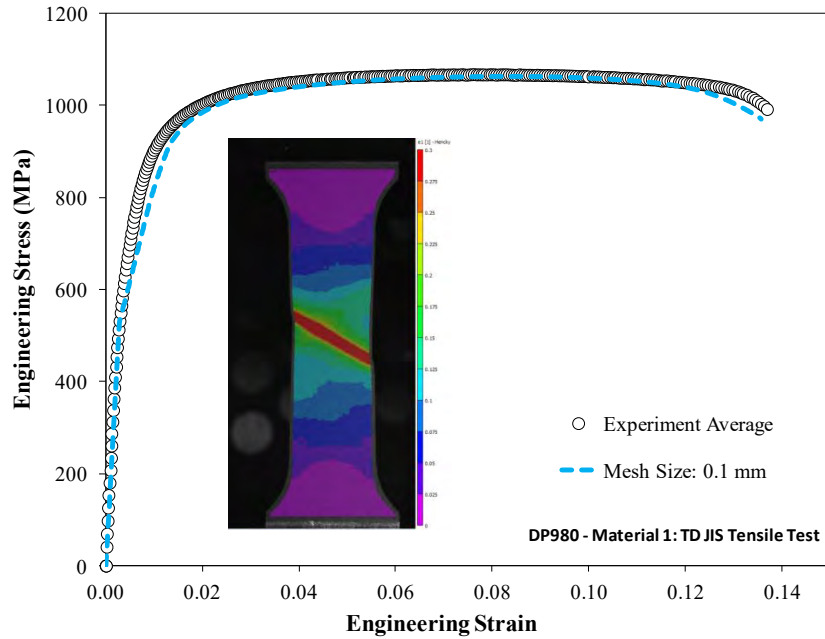
1. Material Characterization at Large Strains *and Strain Rates*

- Tensile characterization from 0.001 to 1000 s⁻¹
 - Scale quasi-static data obtained to large strains for strain rates
- $$\bar{\sigma}(\varepsilon^p, \dot{\varepsilon}^p) = \bar{\sigma}^{QS} \cdot F(\dot{\varepsilon}^p)$$
- Efficient experimental method for constitutive characterization



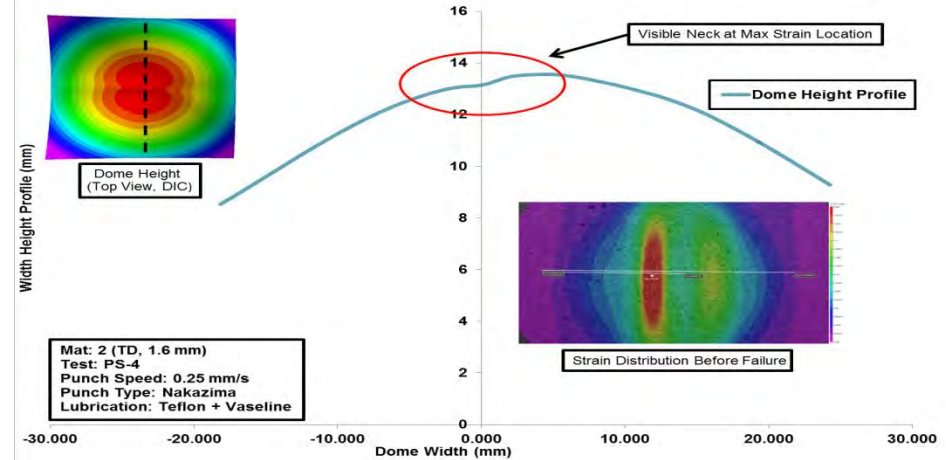
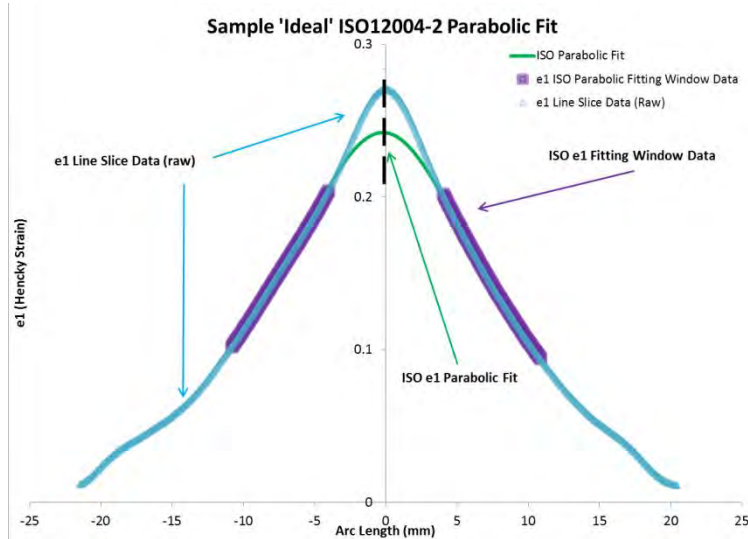
1. Material Characterization at Large Strains *and Strain Rates*

FE Simulations using Experimental Hardening Model and Von Mises Perform Well: **Efficient**



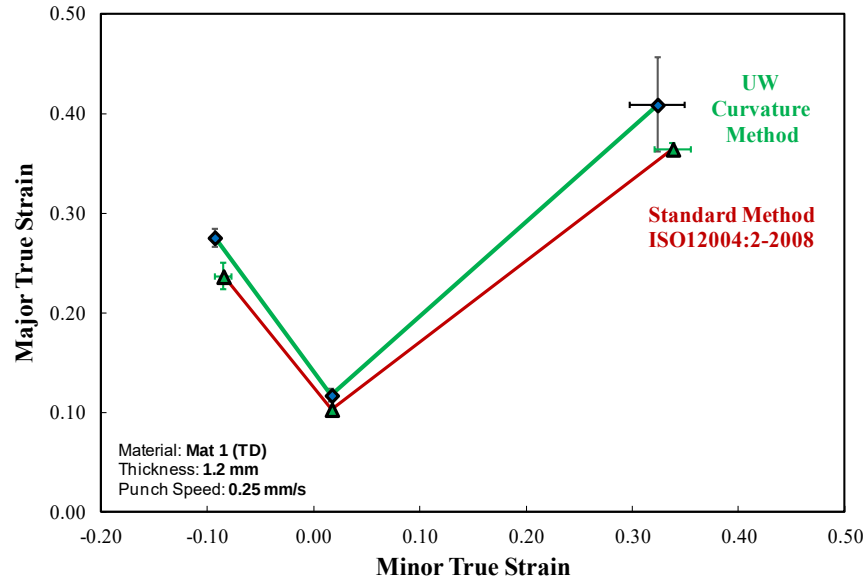
2. Global Formability – FLD Methodology

Physically-motivated FLD detection methods are needed

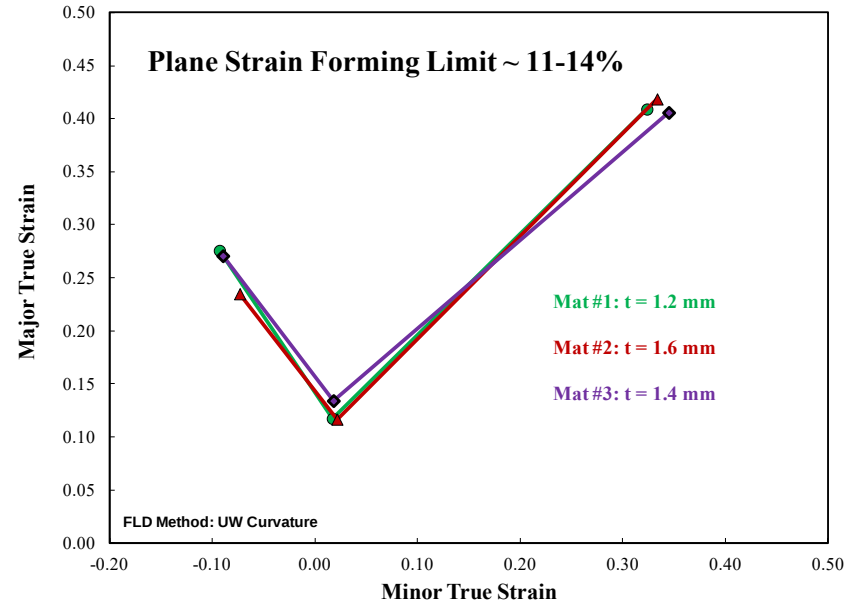


2. Forming Limits

Curvature provides physical upper limit



Comparable FLDs for Three Grades



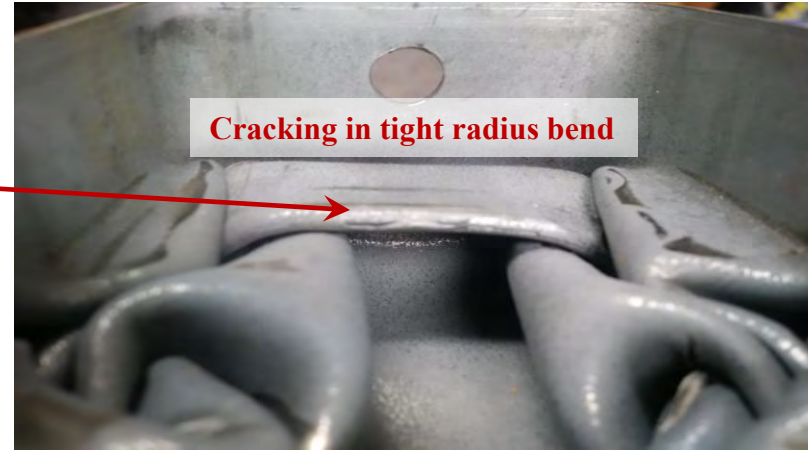
3. Formability and Fracture in Tight Radius Bending

Formability in tight-radius bending identified as key factor in crash performance

VDA 238-100 bend test promising but only reports bend angle



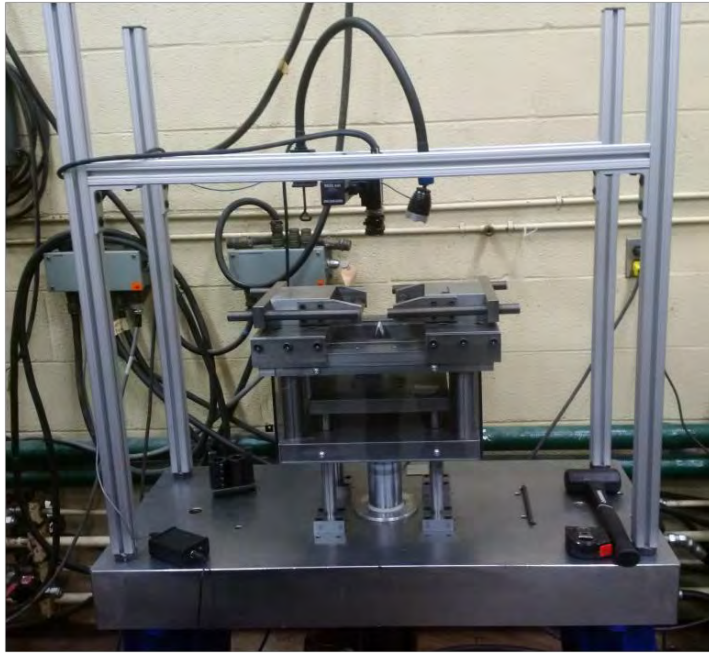
DP980 Material 2
Global Buckling and Folding



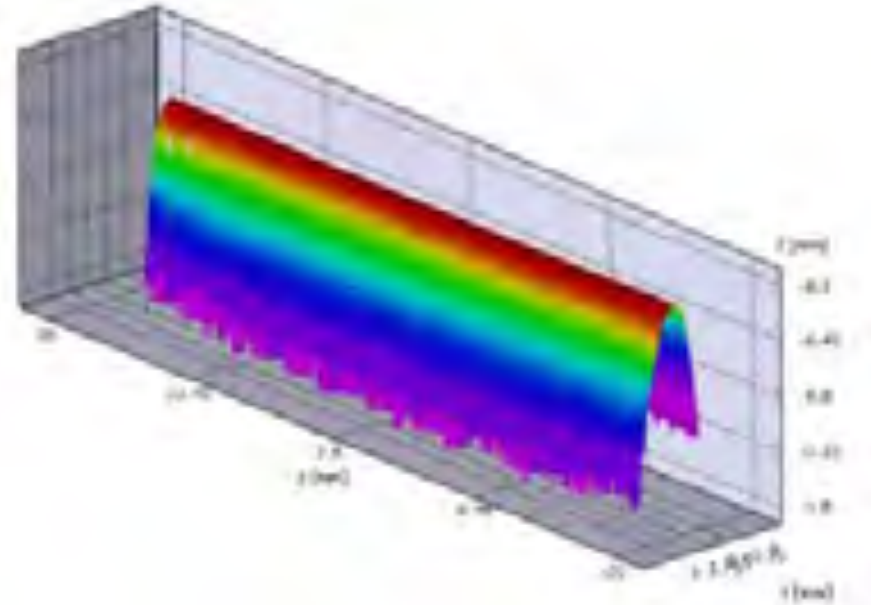
UW-HRA Tailored Hot Stamped Rail
(Omer et al., 2017, Int. J. Impact. Eng)

Optical VDA238-100 Test Frame

UW & HRA Developed an Inverted Bend Test for Optimal DIC Strain Measurement (*IDDRG Conf.*, 2017)



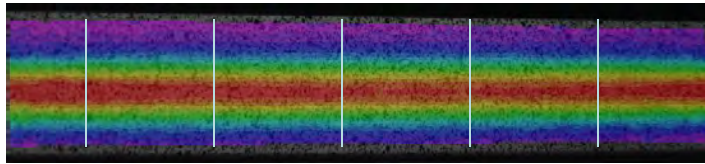
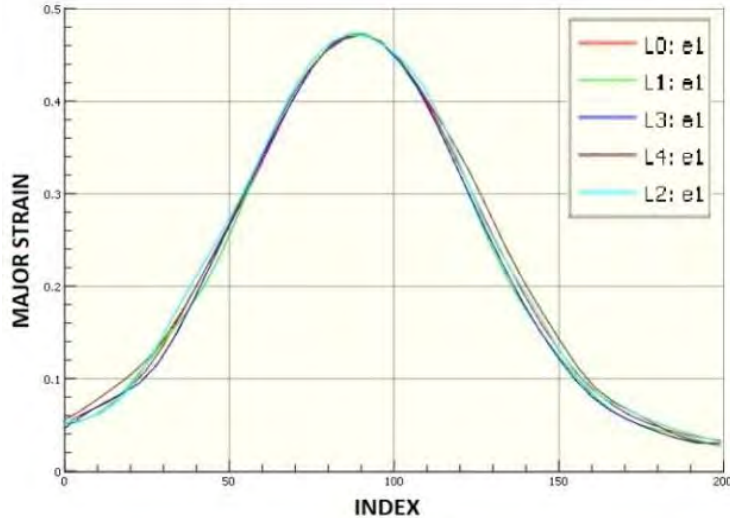
UW's VDA238 configuration with DIC



Measure Fracture Strain & Bend Angle!

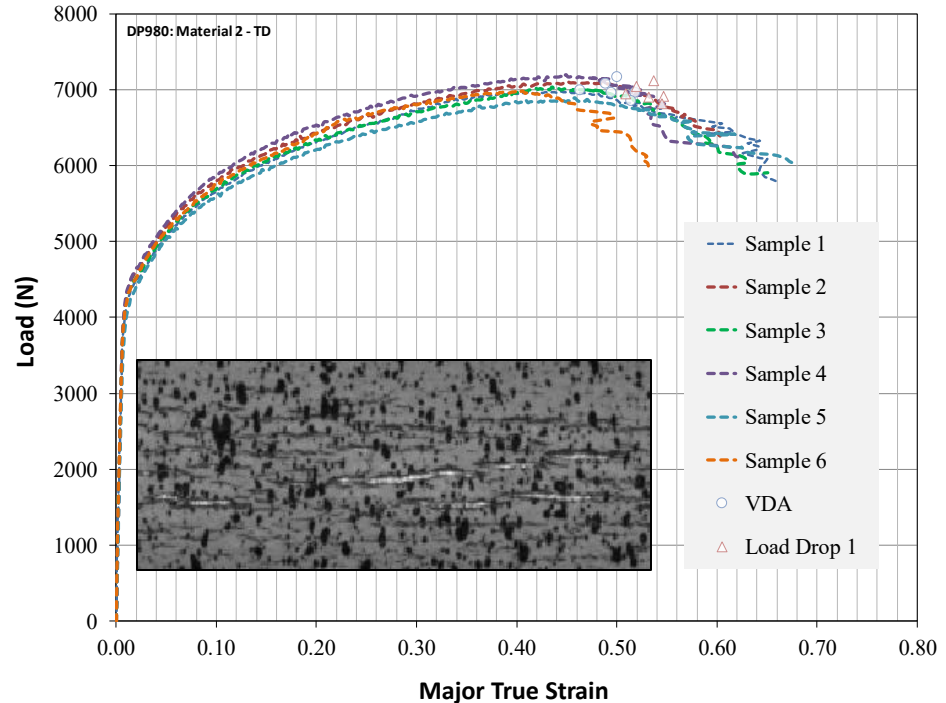
V-Bending with DIC

Homogeneous Strain Distribution along Width



Measures width of specimen (res. < 0.02 mm/pixel)

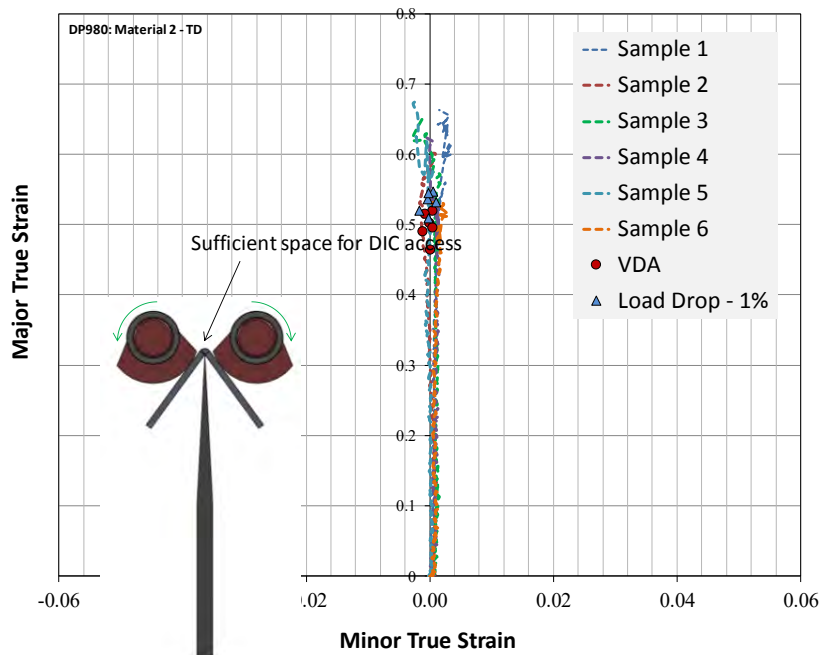
Detect fracture using Load drop (VDA) or visual cracking



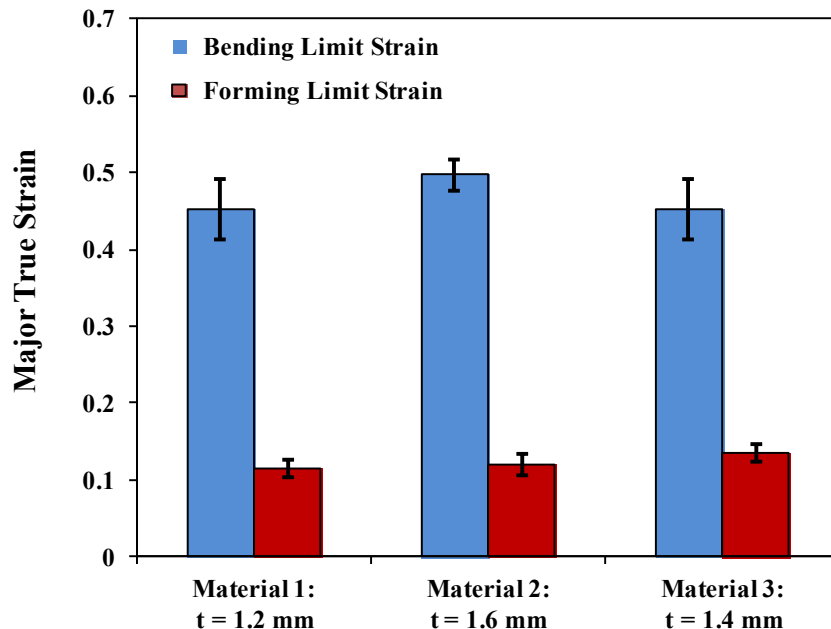
Load vs Major Strain (Ex: 980 Mat#2)

V-Bending with DIC Strain Measurement

**Achieves Ideal Plane Strain Loading
until Onset of Cracking**

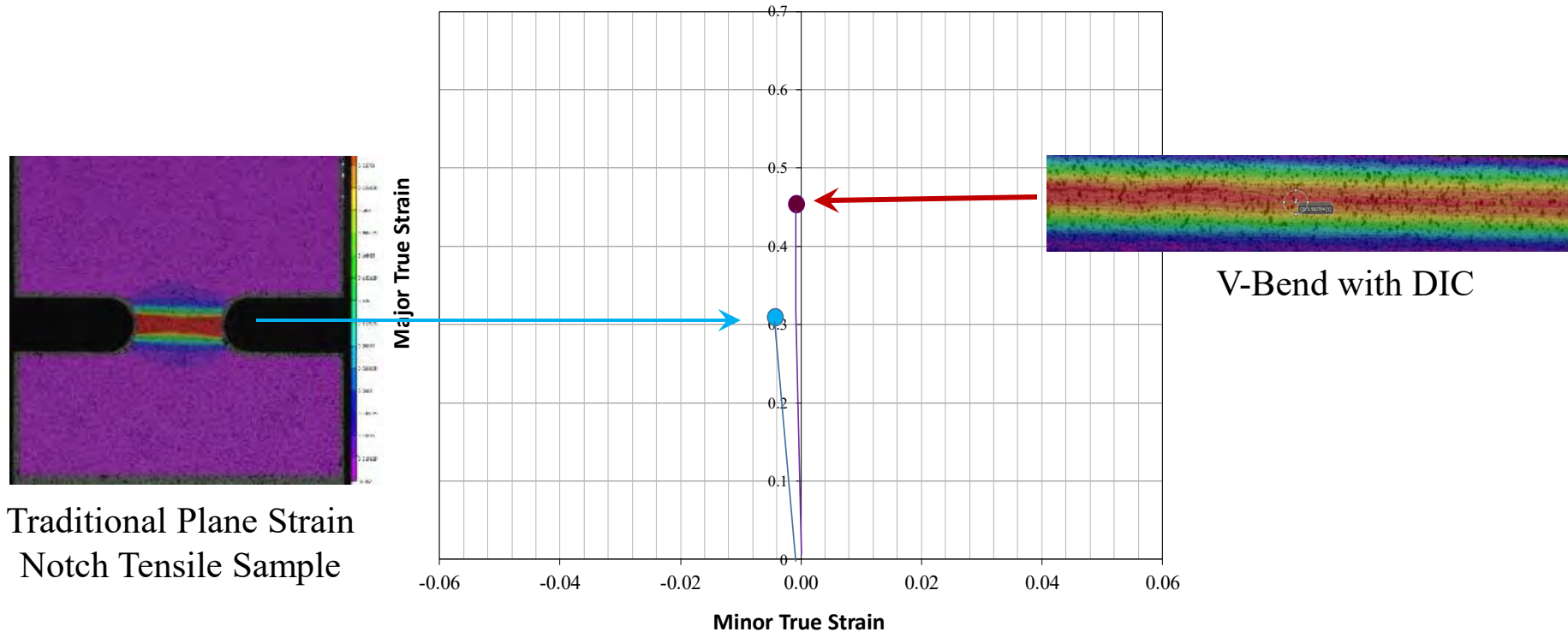


**DP980 Plane strain fracture limits of 45-50%!
Forming limit strains ~ 12%**



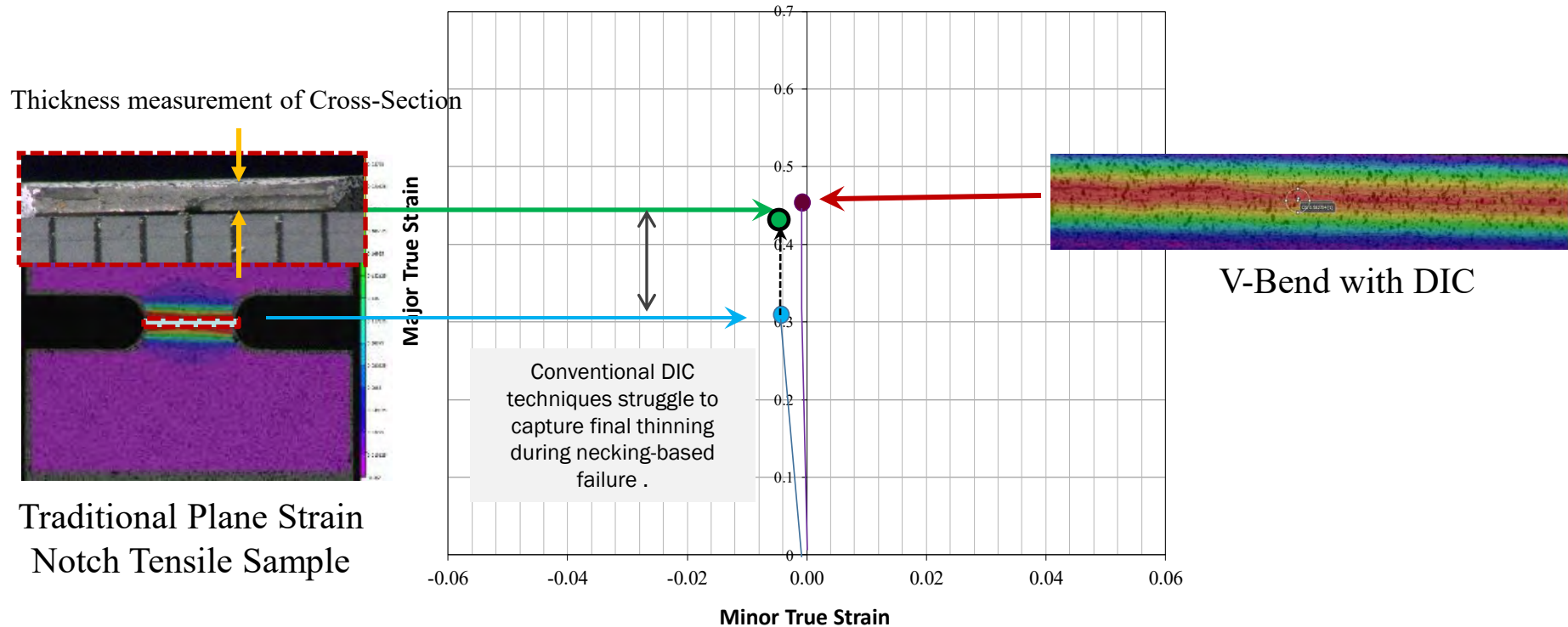
Comparison of V-Bend with Plane Strain Notch

Disagreement between tests: Notch test is lower...



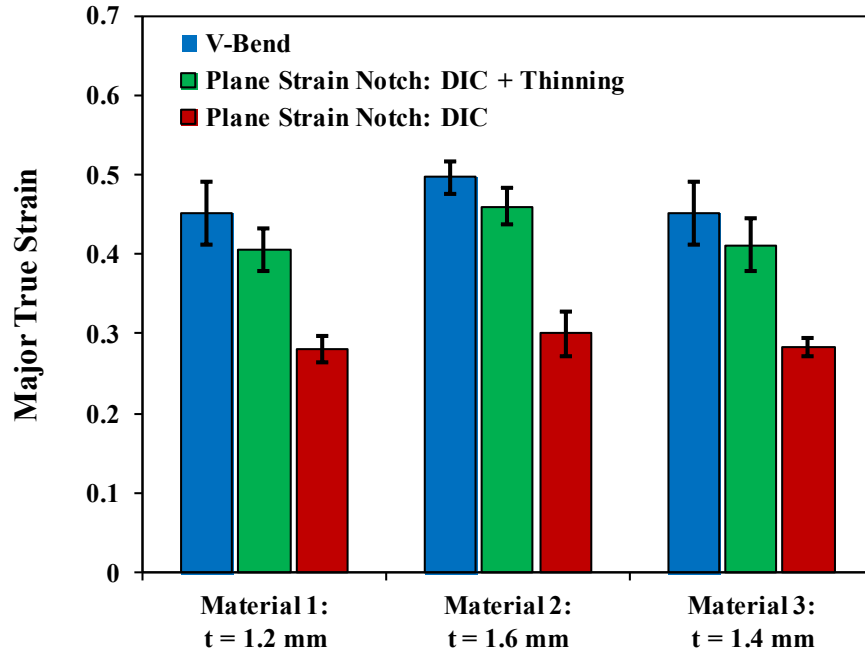
Comparison of V-Bend with Plane Strain Notch

But a thickness correction on the notch resolves the difference



Comparison of V-Bend with Plane Strain Notch

Plane Strain notch provides lower bound estimate if thinning correction performed
Correction also required for plane strain dome tests

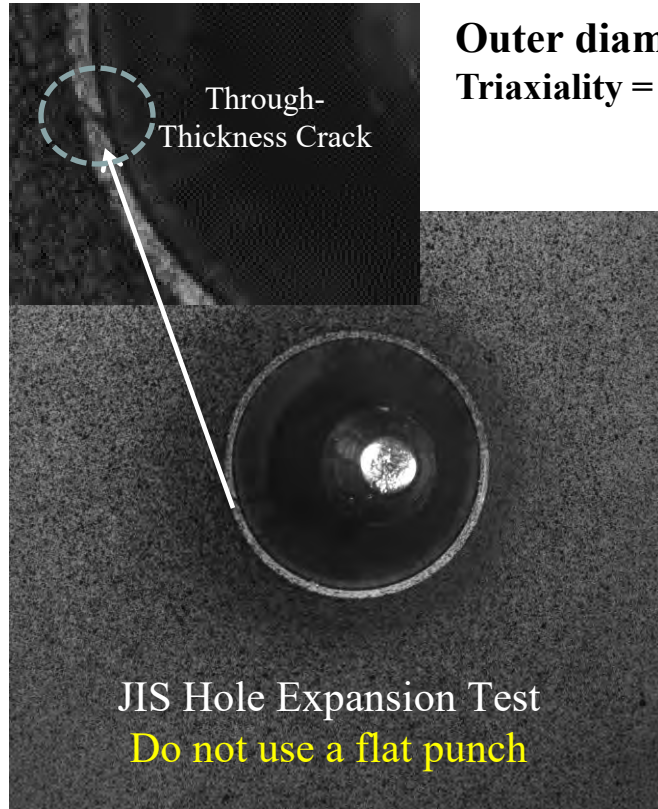


Optical V-Bend Test is Superior

1. No necking
2. Minimal to No Machining
3. Ideal plane strain loading
4. Efficient – low time per test

Conical Hole Expansion Test for Fracture in Uniaxial Tension

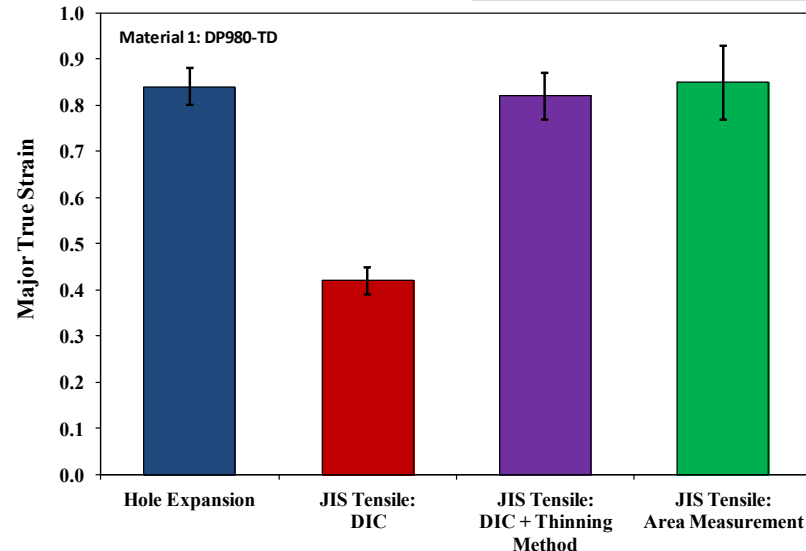
Outer diameter is in uniaxial tension and does not contact the punch
Triaxiality = 1/3 (Butcher et al., SAE, 2013, Pathak et al., JMEP, 2016; Numisheet 2016)



$$HER(\%) = 100 \left(\frac{d_{inner}^f - d_o}{d_o} \right)$$

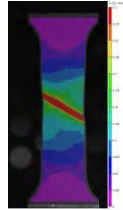
$$\varepsilon_{eq}^f = \varepsilon_c^f = \ln \left(\frac{d_{outer}^f}{d_o} \right)$$

Try it !
You'll like it

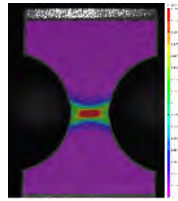


4. Fracture Characterization: 10 Test Geometries

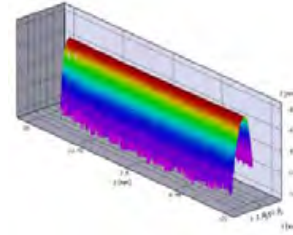
Uniaxial Tension
(Hole Expansion, JIS Tensile)



Intermediary Strain
(3 Notch Tensiles)



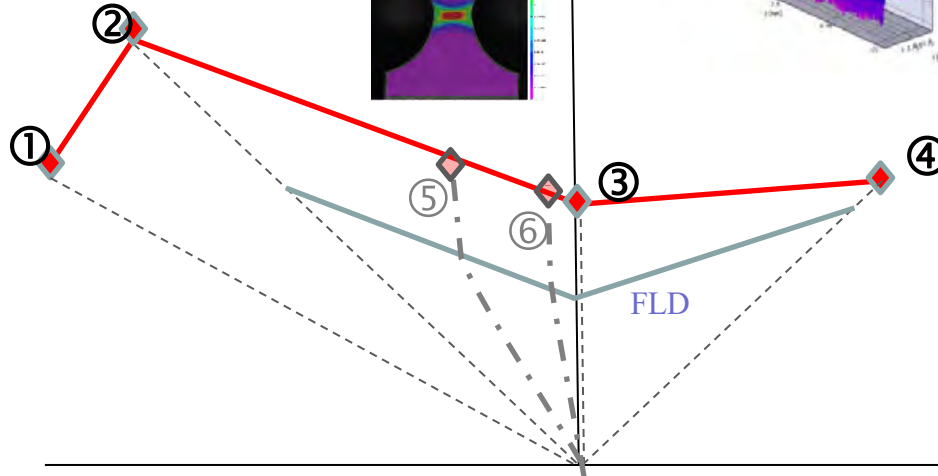
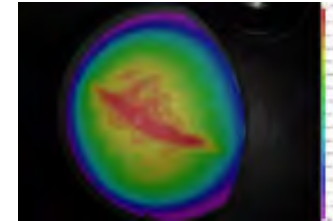
** Plane Strain **
** (V bend) **



Shear
(Mini Shear)

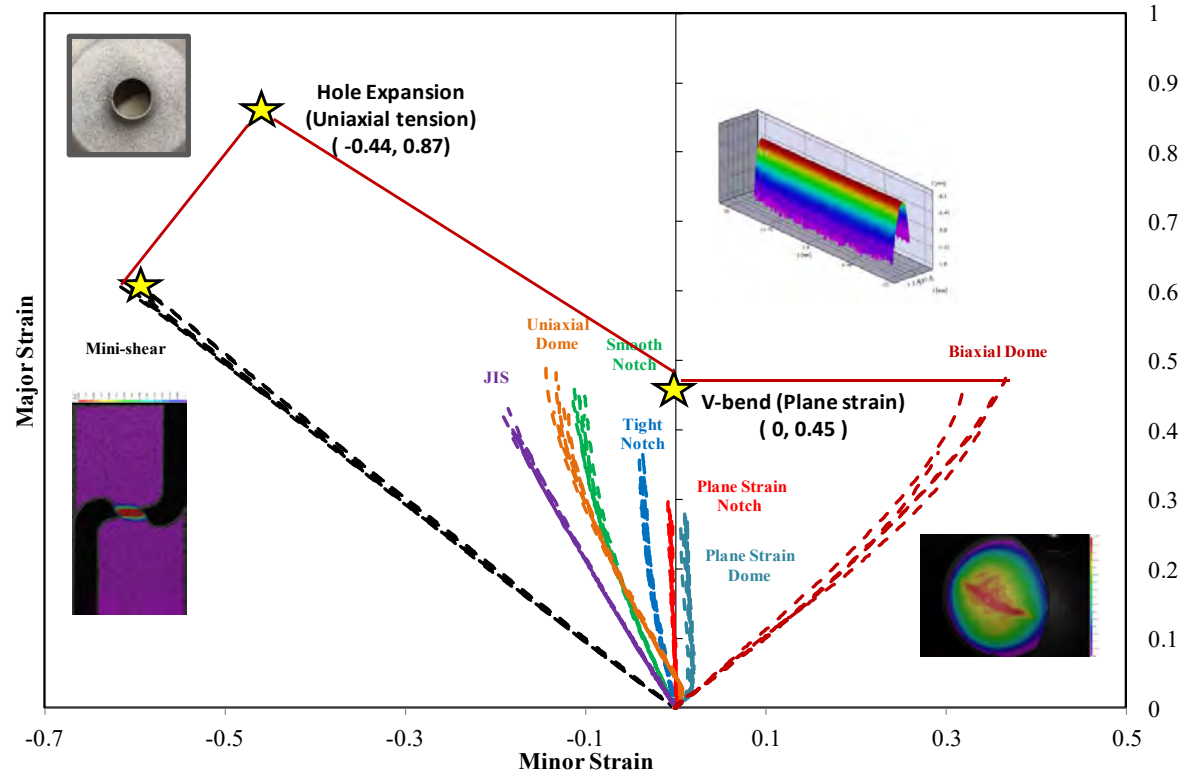


3 Nakazima Dome Tests:
Uniaxial, Plane Strain & Biaxial



4. Fracture Characterization Results

- Conflicting limits provided by different specimen types if thinning correction not applied



Min. of 4 Tests can describe the fracture locus

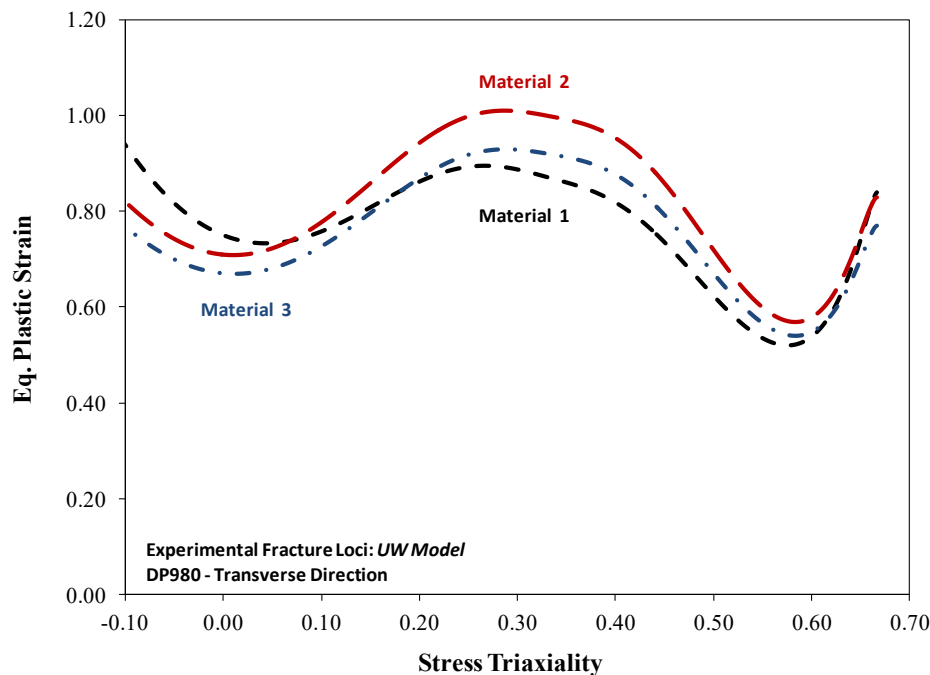
Four Relatively Simple Tests:

1. Mini-shear
2. Hole expansion (reamed)
3. V-Bend
4. Biaxial/Bulge

4. Experimental Fracture Locus

Four tests can be used to generate physically-meaningful fracture loci

Not the product of a simulation exercise – Real material performance can be assessed

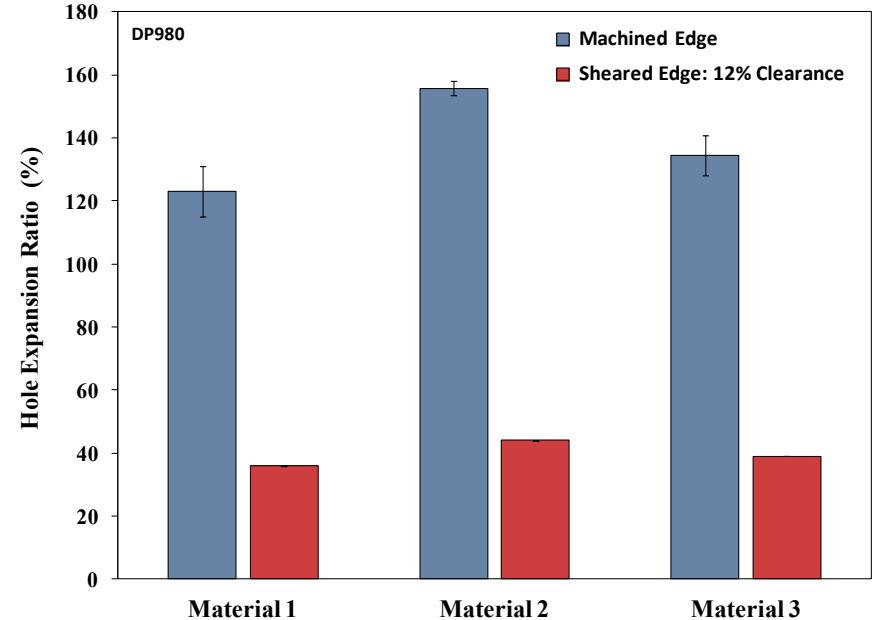
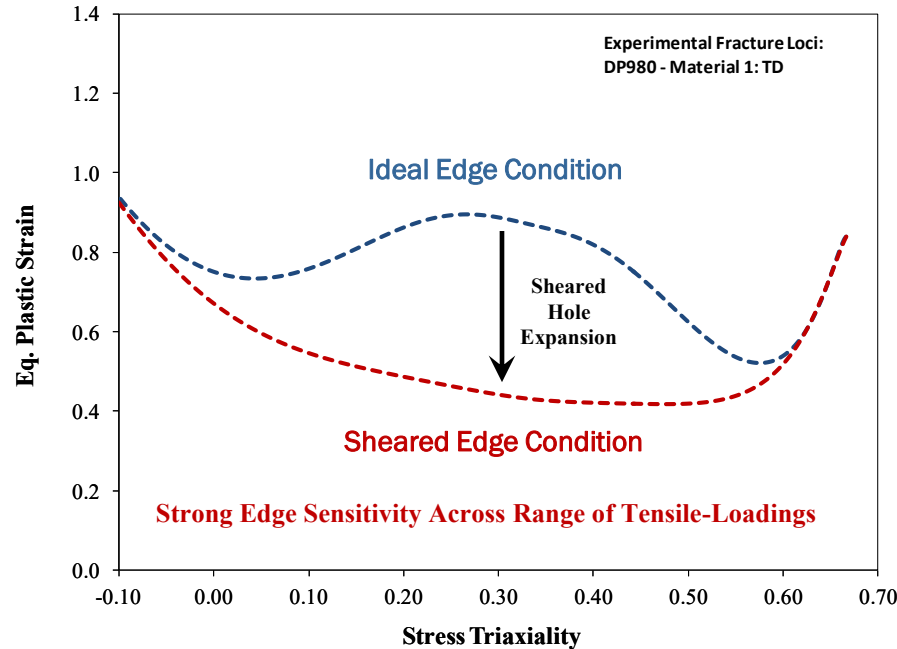


- Relatively comparable fracture loci
- Mat 2 had the *lowest hardening rate*, *highest hole expansion* and *v-bend*

4. Experimental Fracture Locus with Edge Effects

Sheared Edge Failure is a Uniaxial Tensile Mode:

Use Punched Hole Expansion Tests to Obtain Uniaxial Failure Strain with Sheared Edge



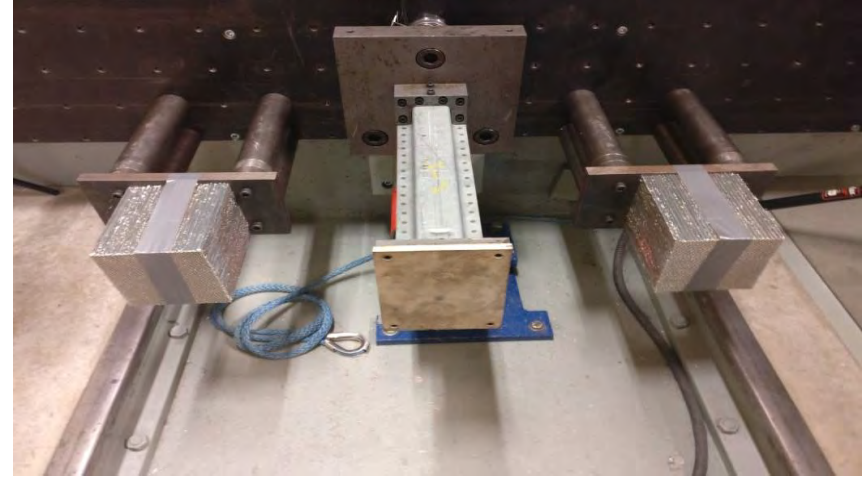
Dynamic Structural Component Evaluation

3-Point Bend Dynamic Crash Test at UW



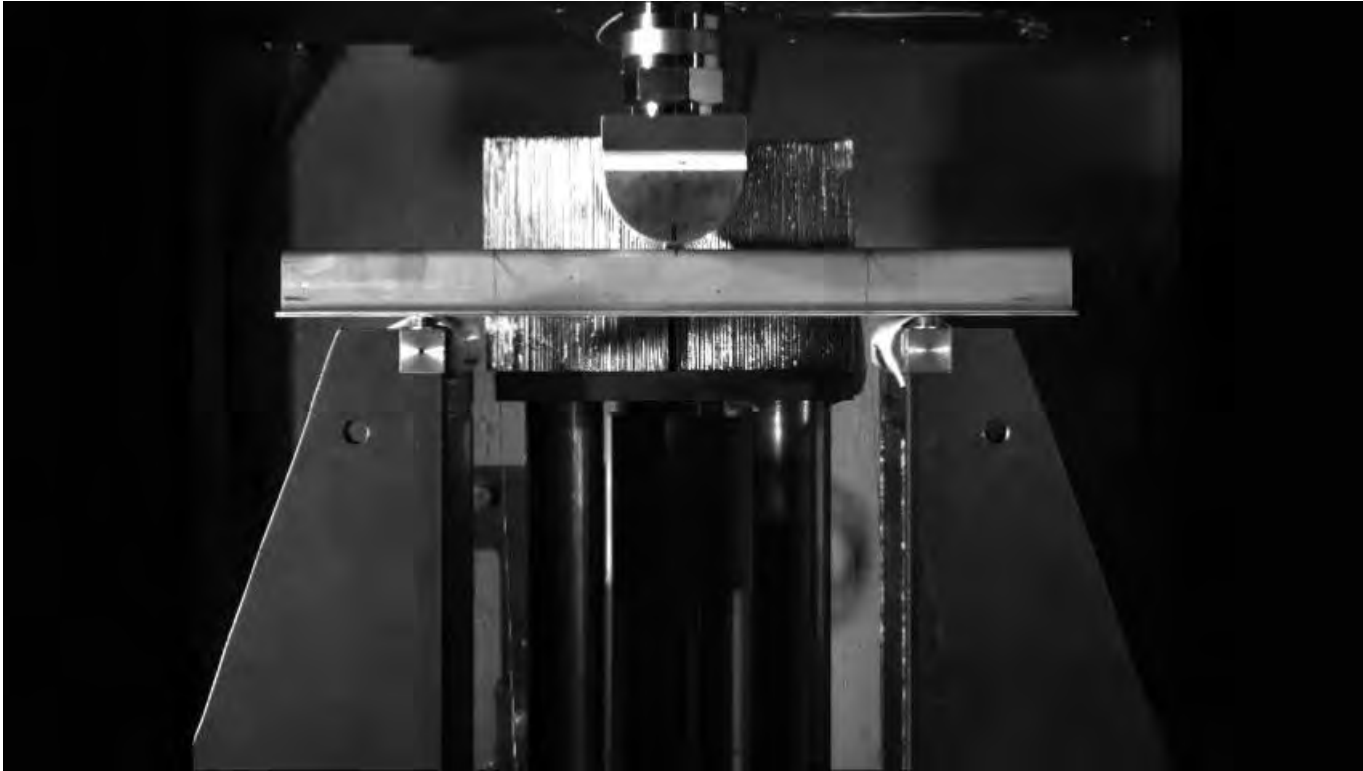
- Sled Mass: 855kg
- Sled Velocity: 25.5km/h
- Total Energy: 21kJ
- Free Crush Distance: 100mm
- Total Crush Distance: 160mm

Axial Crush Dynamic Crash Test at UW



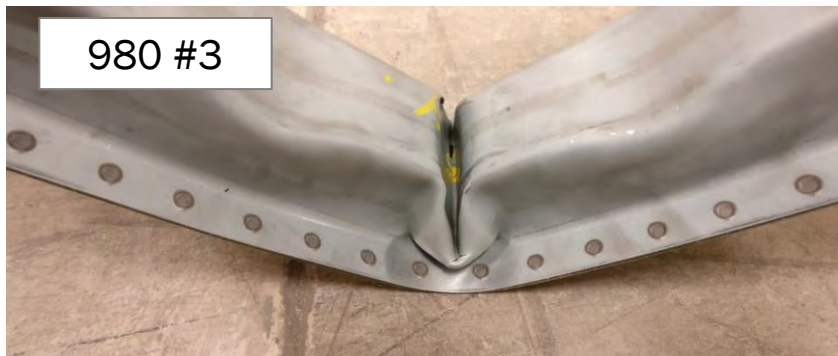
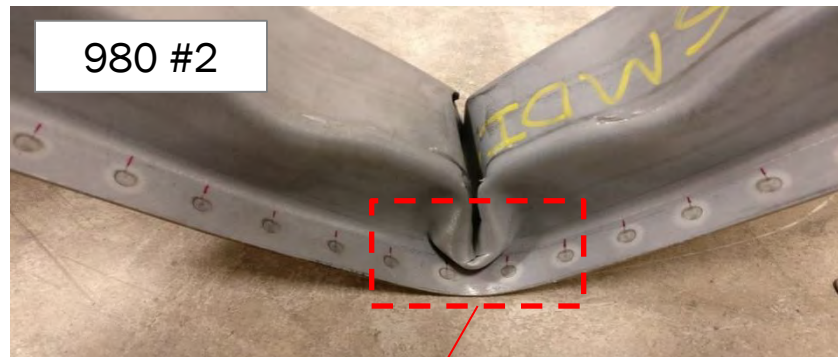
- Sled Mass: 855kg
- Sled Velocity: 25.5km/h
- Total Energy: 21kJ
- Free Crush Distance: 115 mm
- Total Crush Distance: 135mm

Dynamic 3-Point Bend Test at UW



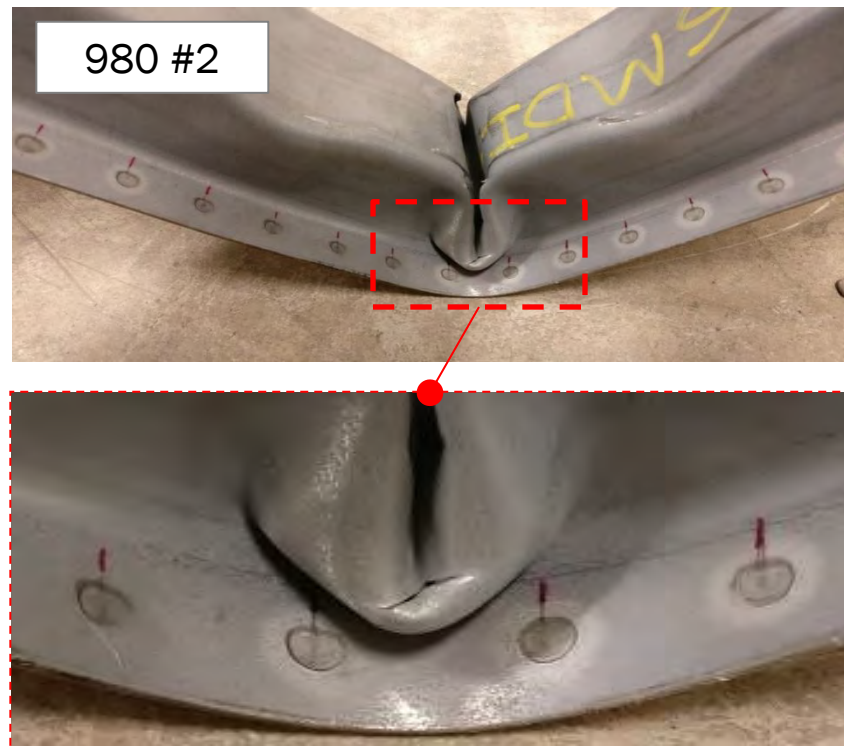
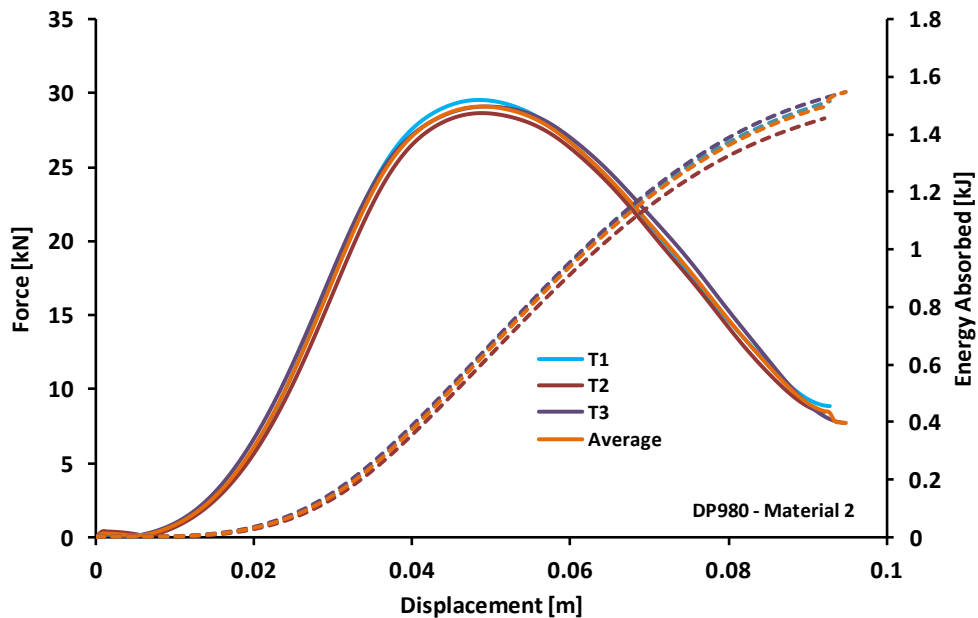
Dynamic 3-Point Bend Test Results

Minimal Cracking for the 3 Grades

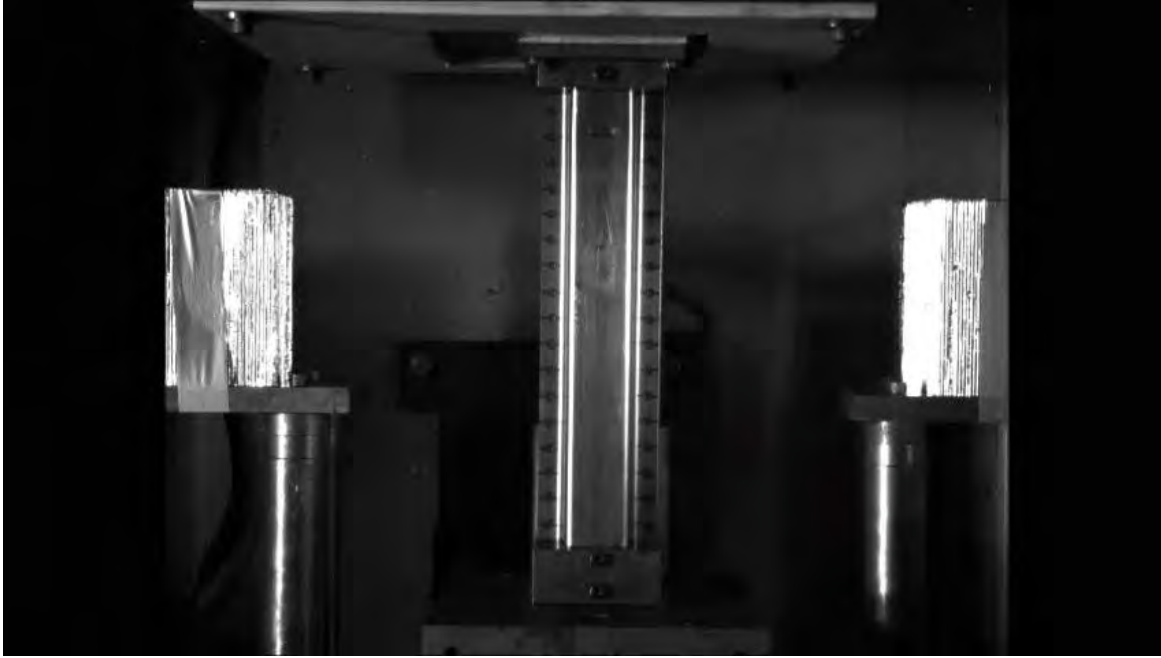


Dynamic 3-Point Bend Test Results: Mat. 2

Minor cracking not detected in load response



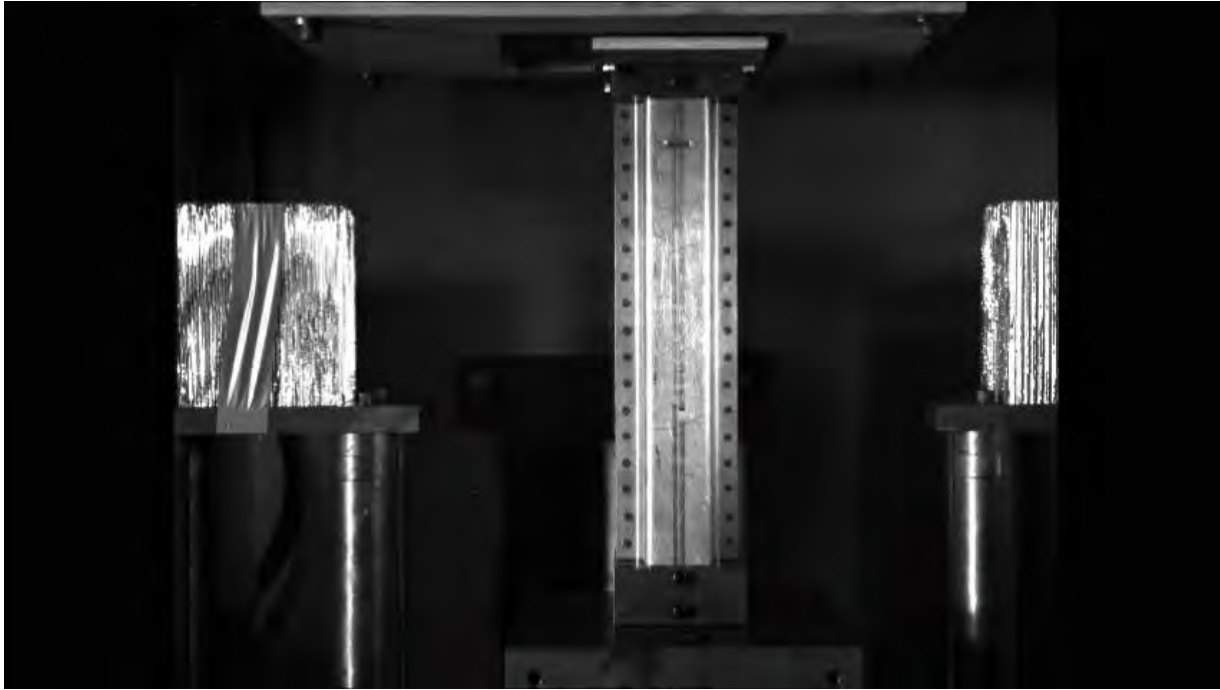
Dynamic Axial Crush Test: Material 1



Material #1: $t = 1.2 \text{ mm}$



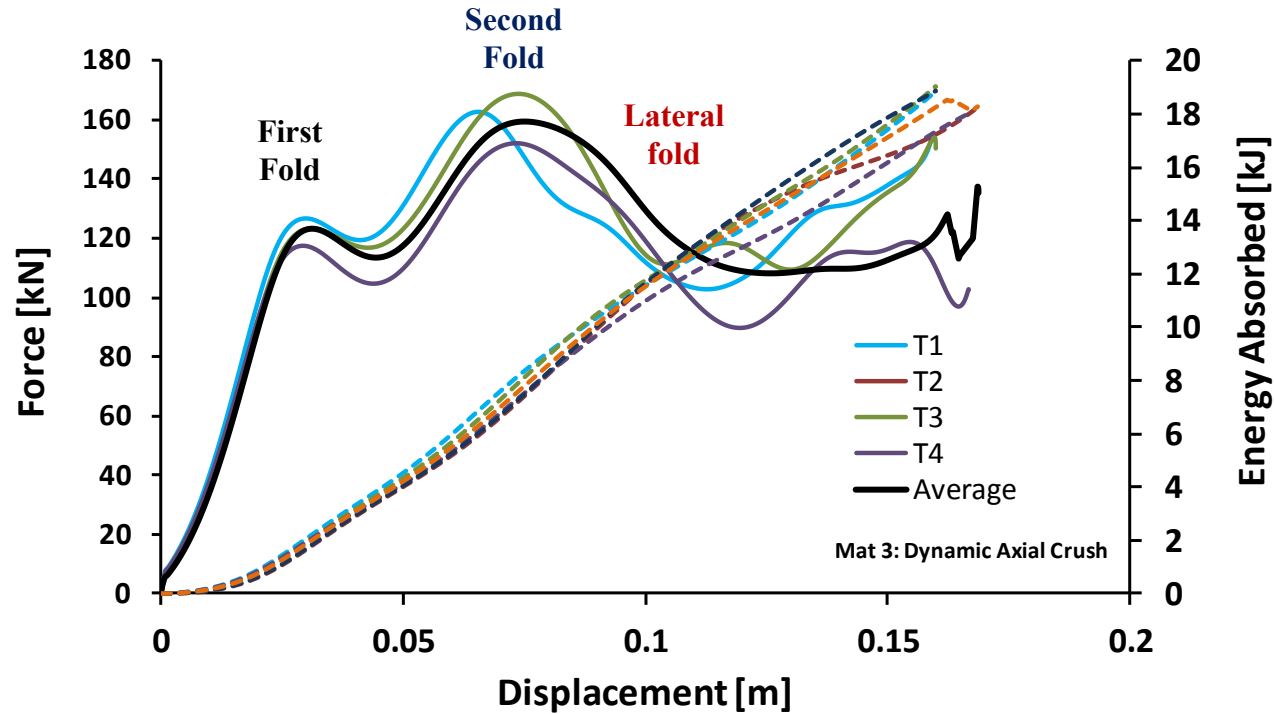
Dynamic Axial Crush Test: Material 3



Material #3: $t = 1.4 \text{ mm}$



Dynamic Axial Crush Test: Material 3



Dynamic Axial Crush Test Results



Material #1: $t = 1.2$ mm



Material #2: $t = 1.6$ mm



Material #3: $t = 1.4$ mm

**Relatively Good
Performance for 3 Grades**

**Repeatable Energy
Absorption**

**Material 3 had highest
spot weld strength and
strain rate sensitivity**

Efficient and Accurate Experimental Methodologies Established for Characterization of AHSS

1. Method to experimentally obtain hardening to large strains and strain rates
2. New FLD detection algorithm: Curvature-based
3. Optical V-Bend developed: Ideal plane strain test
4. Four tests required to efficiently obtain fracture locus for a material

As with FLD's, Use 4 Industrially Friendly Tests to Construct Fracture Locus to Compare Material Performance → Accounts for Edge Condition

New model to use four tests for rapid FE model implementation → Next GDIS

For More Information

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