

# GREAT DESIGNS IN **STEEL**

## THE DIC REVOLUTION IN METAL PROPERTY CHARACTERIZATION

Dr. Thomas B. Stoughton

GM Global R&D Center, GM Tech Fellow



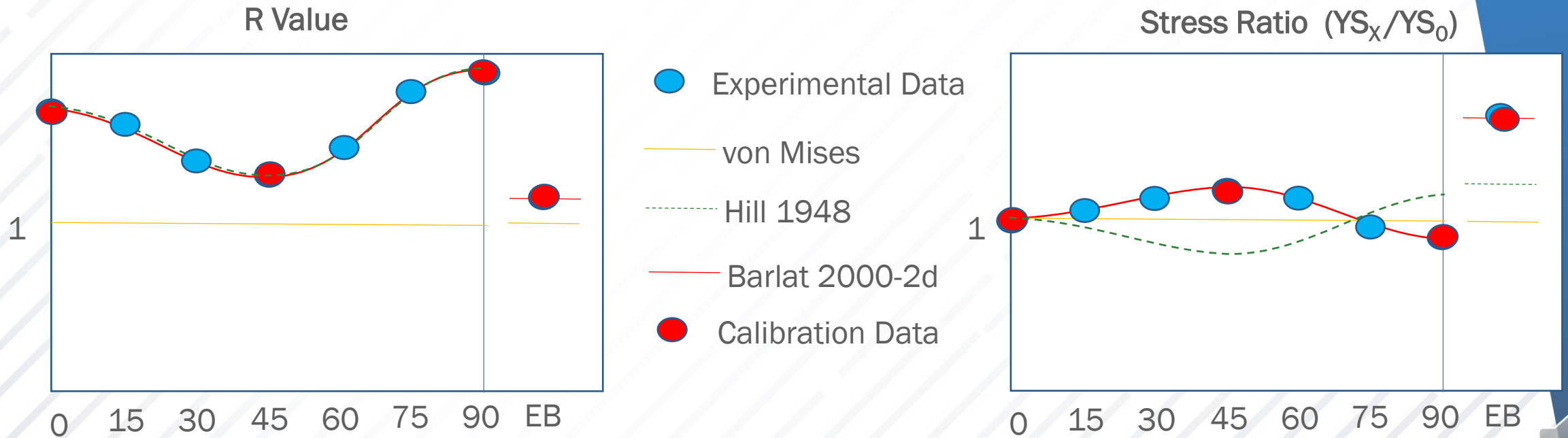
# MOTIVATION

- 1) Why is a revolution in material testing needed?
- 2) What is revolutionary about Digital Image Correlation?
- 3) What is the potential of a SINGLE Uniaxial Tension Test?
  - Example of DP 980



# HISTORY OF CONSTITUTIVE MODELS

- 1) Von Mises Yield Model (1913) ← Requires only a single hardening law
- 2) Hill 1948 Fully Anisotropy Model ← ... also requires  $R_0, R_{45}, R_{90}$
- 3) Barlat 2000-2d Model ← ... also requires  $YS_0, YS_{45}, YS_{90}$  and  $YS_{EB}$ , and  $R_{EB}$



# TRADITIONAL UNIAXIAL TENSION TEST

## Standard Results

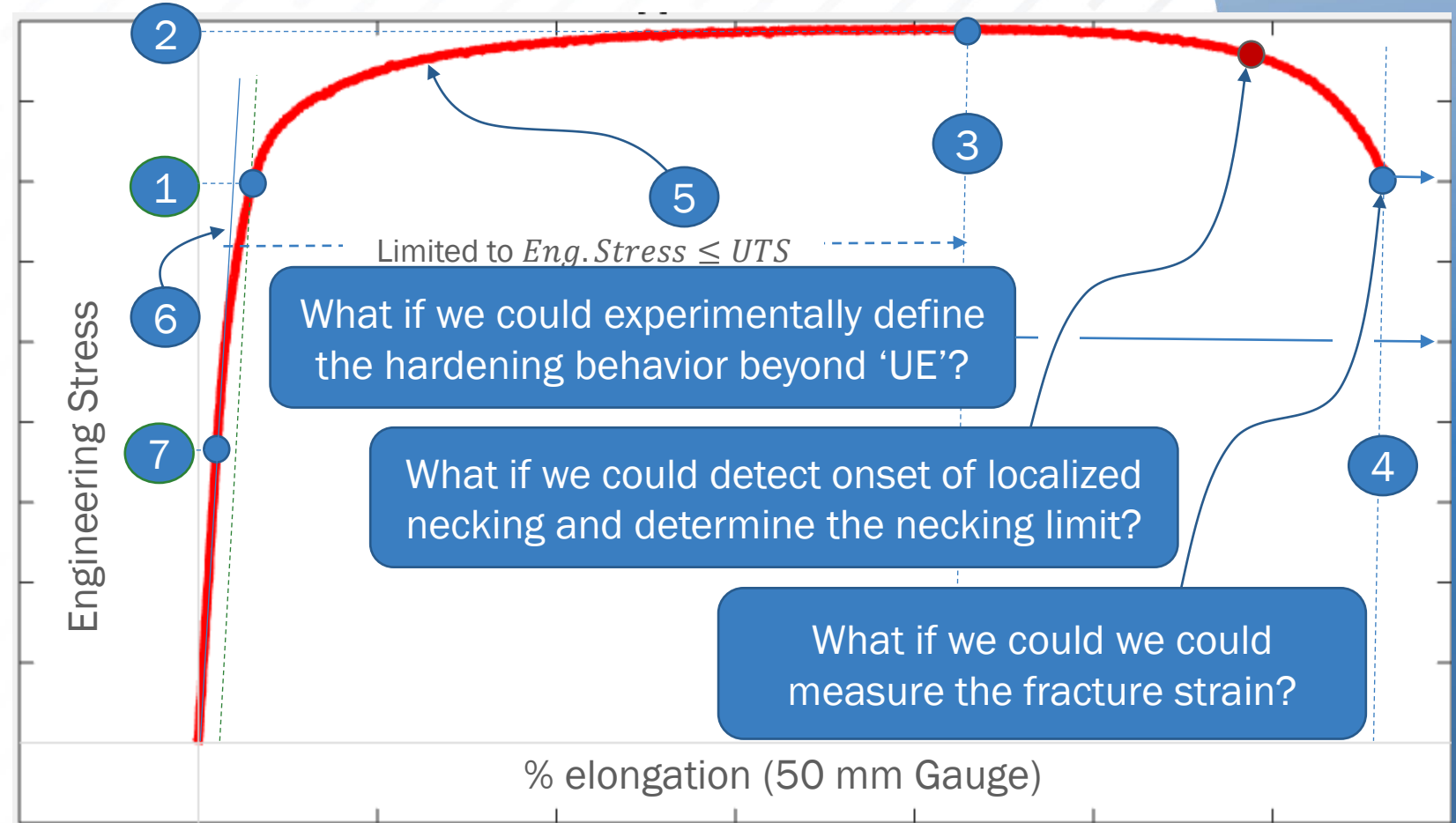
- 1) 0.2% Offset Yield Stress
- 2) Ultimate Tensile Strength
- 3) Uniform Elongation
- 4) Total Elongation
- 5) Hardening Behavior
- 6) Elastic Modulus
- 7) Proportional Limit

## Add a Width Strain Gauge

- 8) R Value
- 9) Poisson Ratio

## Additional Needs

- 10) m Value (jump tests)
- 11) YM degradation (load/unload)
- 12) Property variation (repeats)



Additional Tension Tests

What if we could get a handle on this from a SINGLE Uniaxial Tension Test?

# HOW TO BEST USE DIC

## Standard Results

- 1) Young's Modulus
- 2) Ultimate Tensile Strength
- 3) Uniform Elongation
- 4) Hardening Behavior
- 5) Total Elongation

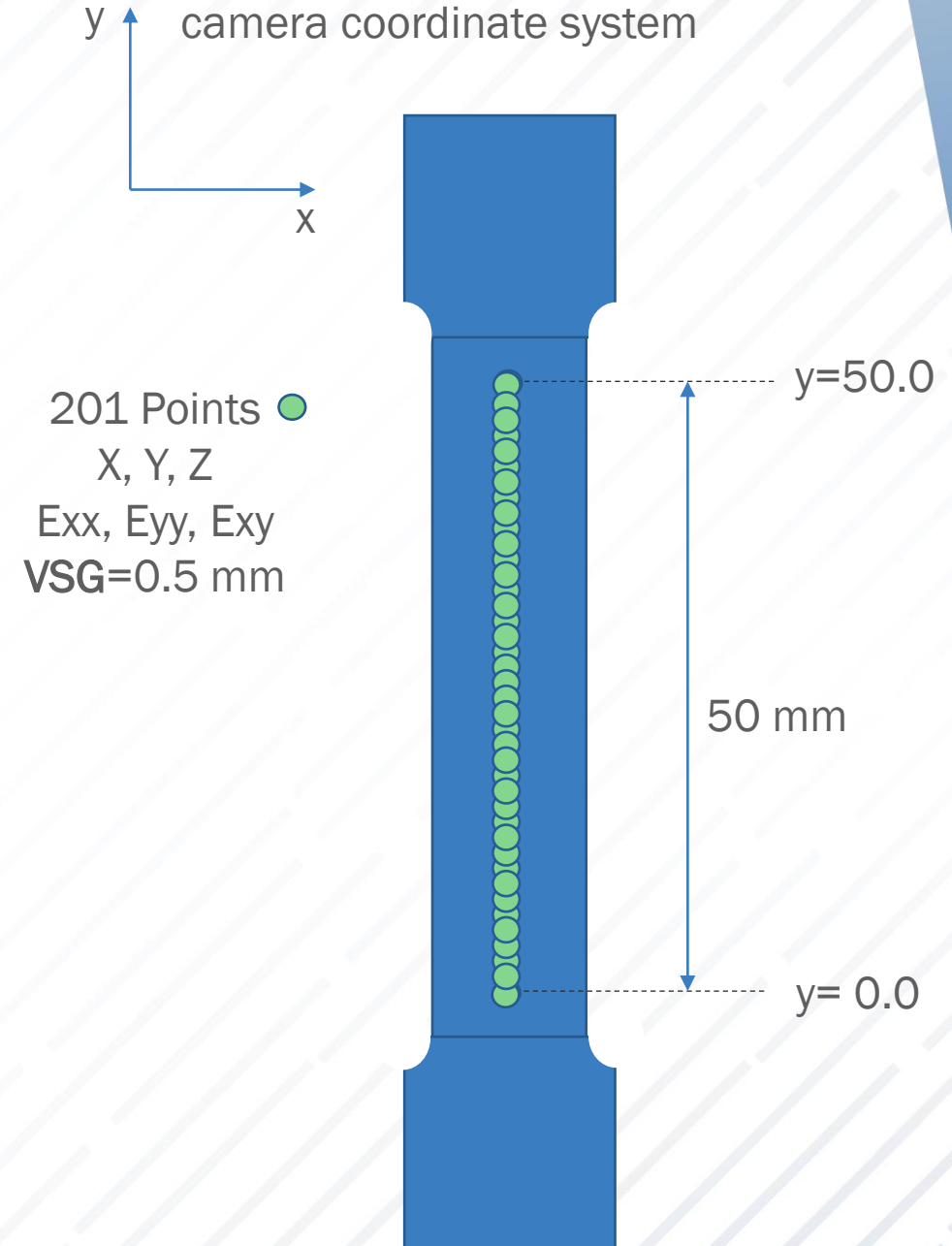
## Includes Width Strain Gauge

- 6) R Value
- 7) Poisson Ratio

## Implicitly Includes Multiple Loading Conditions

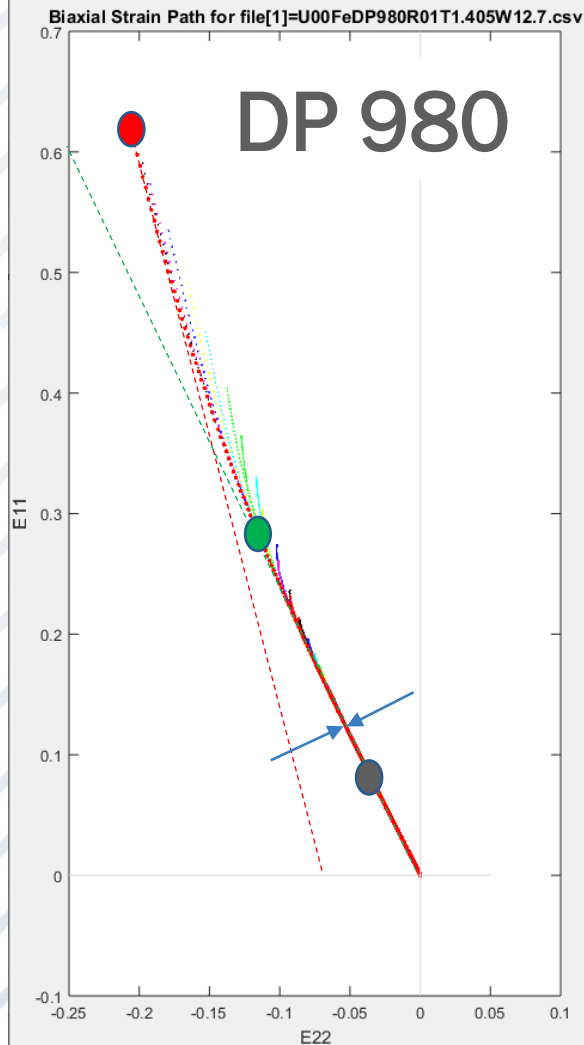
- 8) m Value (jump tests)
- 9) YM degradation (load/unload)
- 10) Property variation (repeats)

## Multiple Points



# R VALUE MEASUREMENT

## 201 Strain Paths



## Benefits of DIC

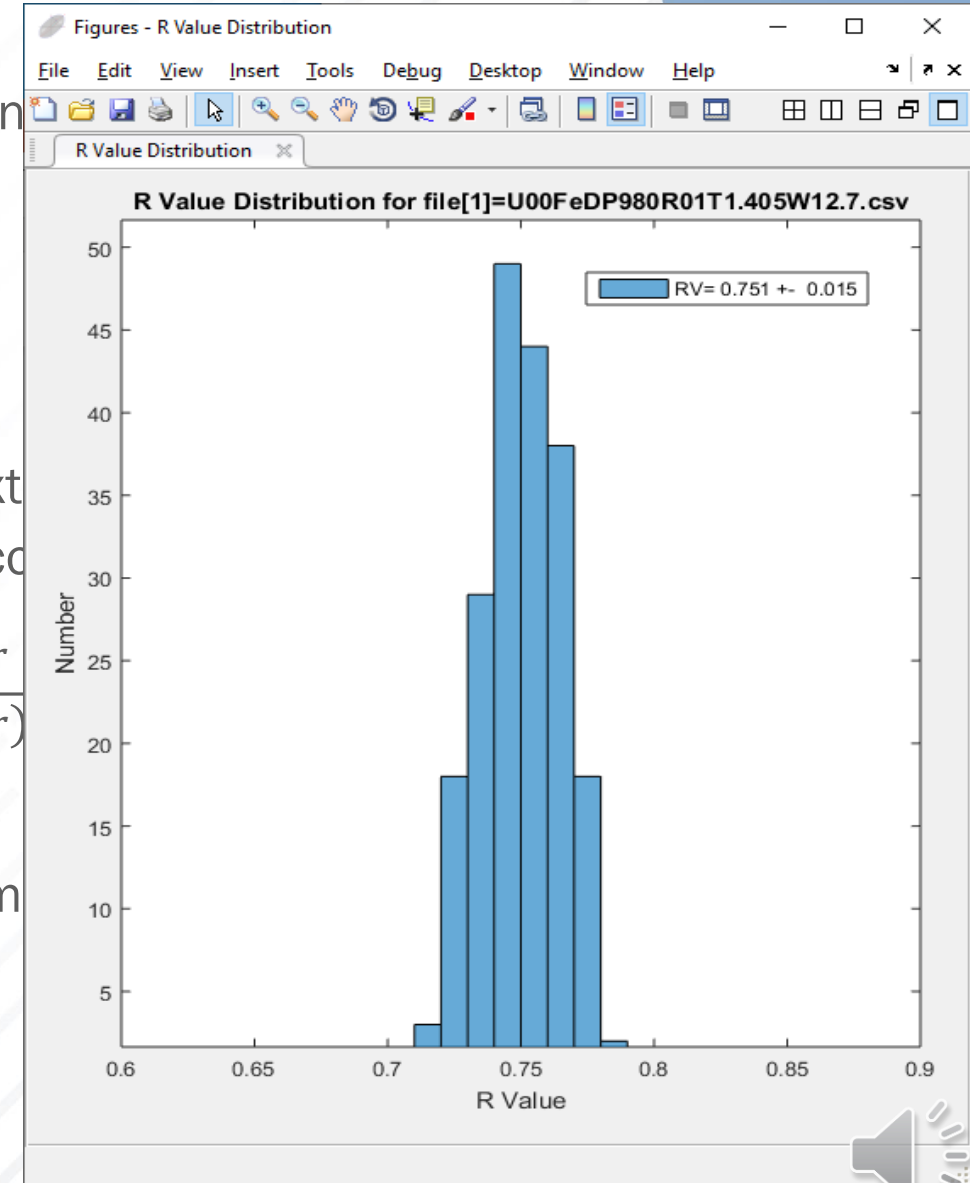
- 1) R Value can be defined properly, in terms of ratios of plastic strain rates

$$slope = -\frac{1+r}{r}$$

- 2) Change in slope is attributed to
  - Change in R Value (crystal texture)
  - Rise of Non-uniaxial tension component
  - Both

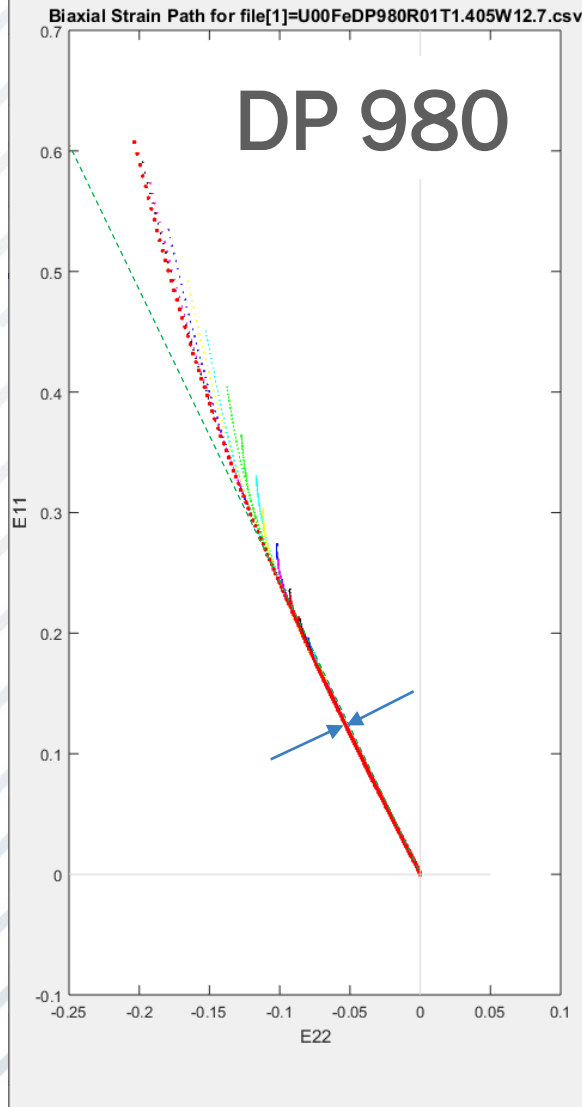
$$slope = -\frac{1+r+\alpha r}{r+\alpha(1+r)}$$

- 3) No noise in 201 Strain Paths → Insignificant error using the 0.5 m
- 4) R Value at 201 points provides material variation information

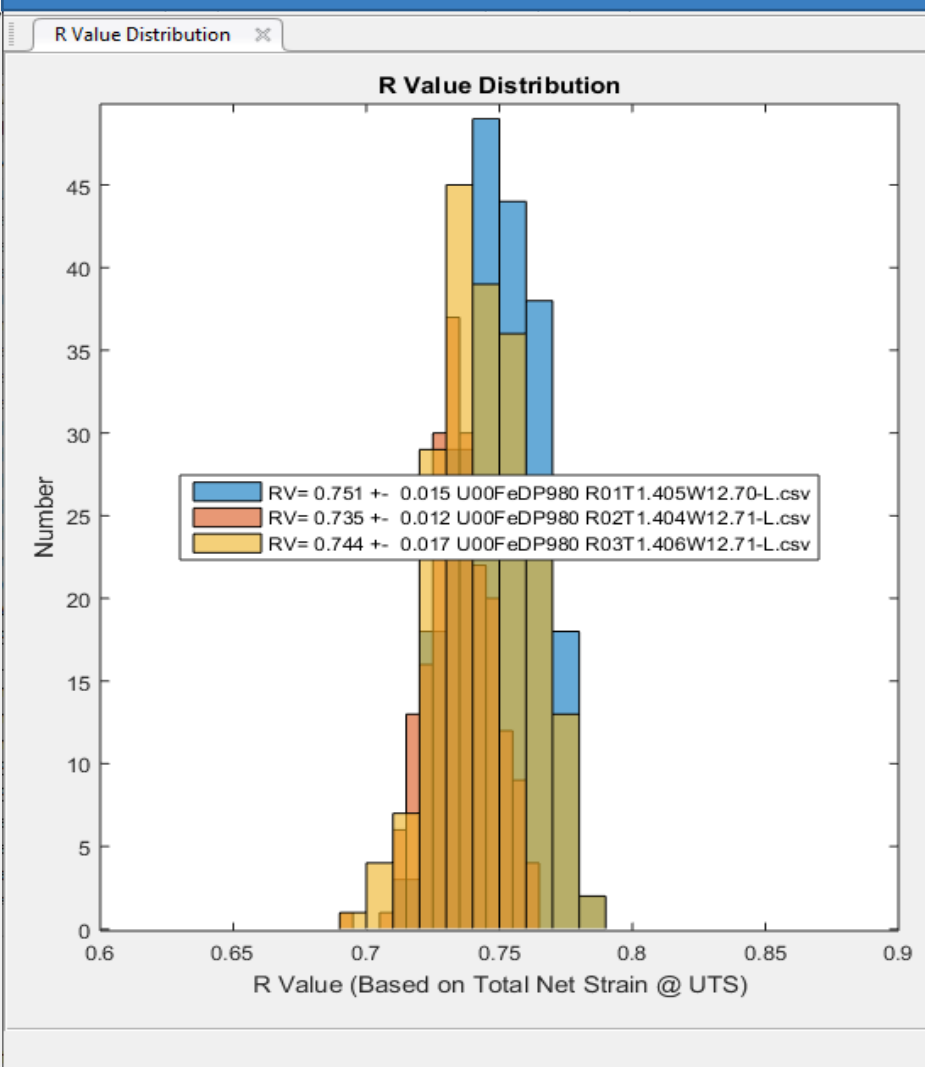


# R VALUE MEASUREMENT

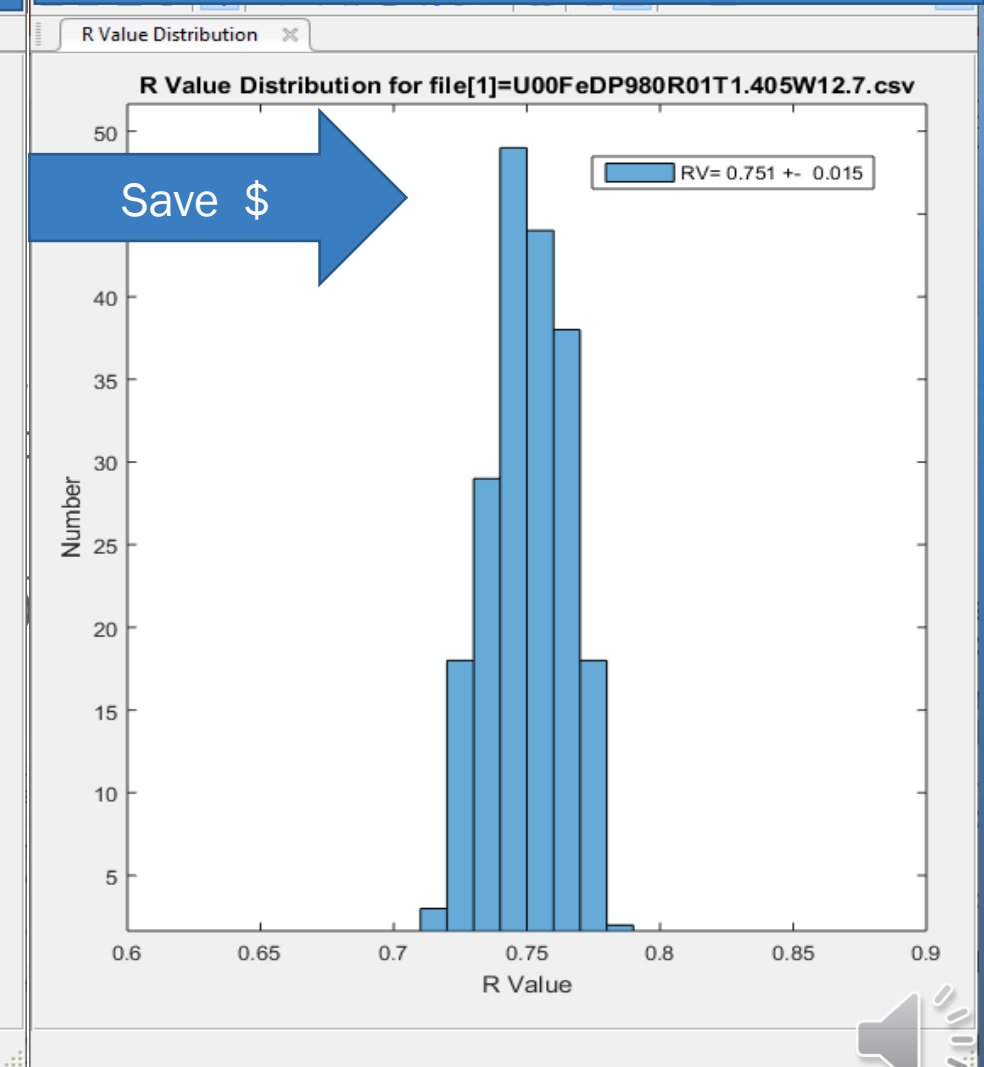
## 201 Strain Paths



## 3 Tests with 603 R Values



## 1 Test with 201 R Values



# HOW TO BEST USE DIC

## Standard Results

- 1) Young's Modulus
- 2) Ultimate Tensile Strength
- 3) Uniform Elongation
- 4) **Hardening Behavior**
- 5) Total Elongation

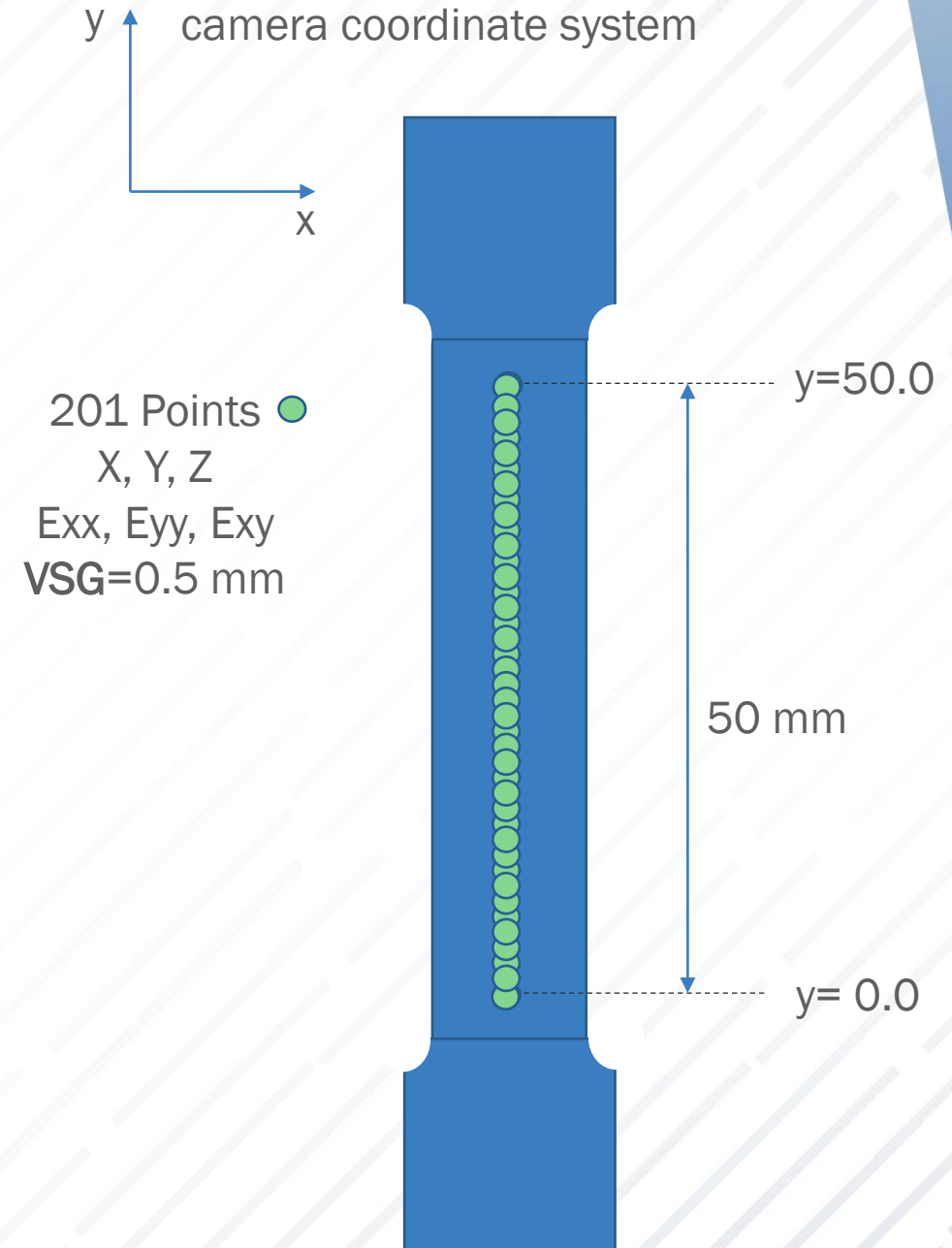
## Includes Width Strain Gauge

- 6) R Value
- 7) Poisson Ratio

## Implicitly Includes Multiple Loading Conditions

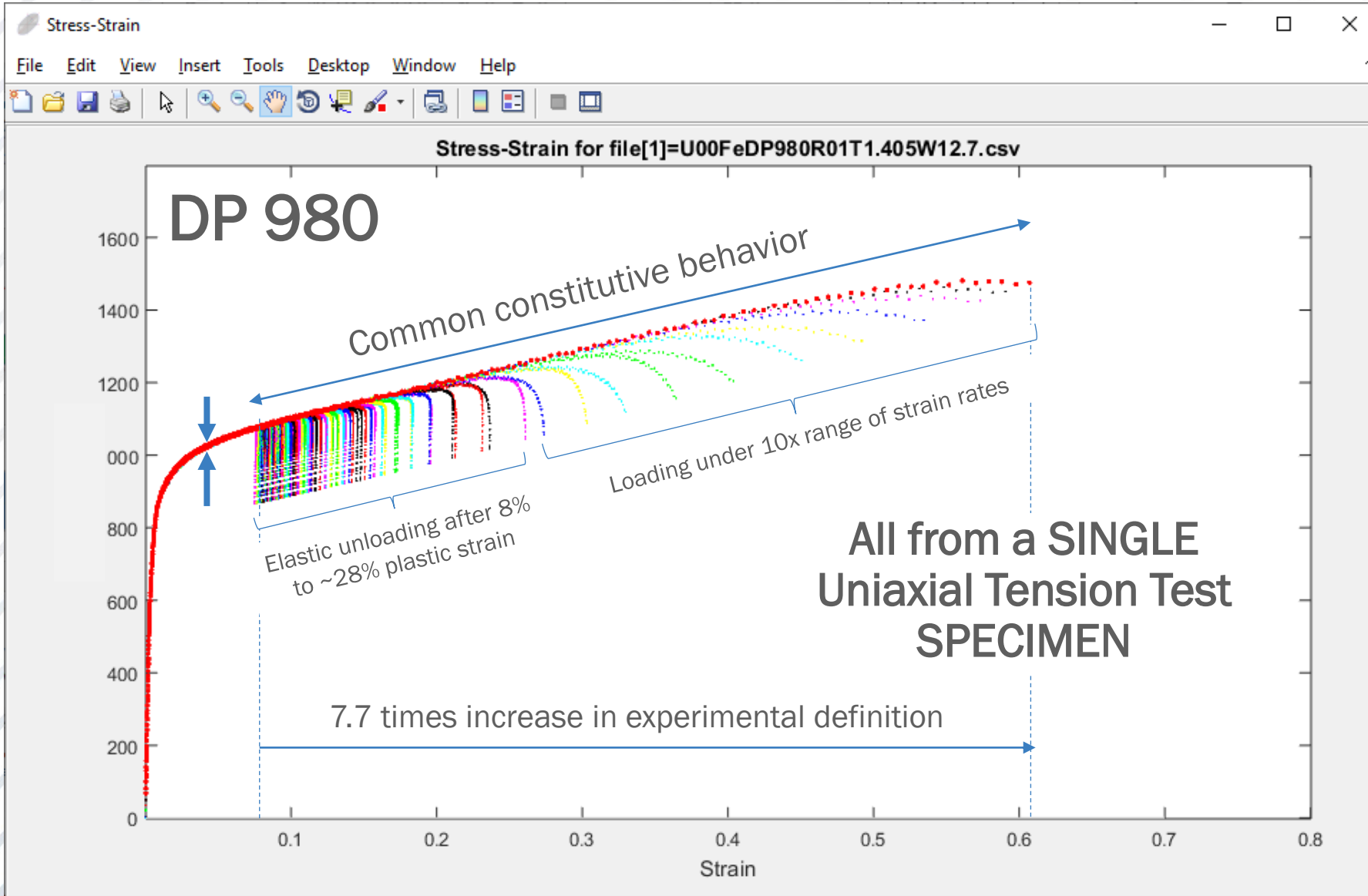
- 8) m Value (jump tests)
- 9) YM degradation (load/unload)
- 10) Property variation (repeats)

## Multiple Points



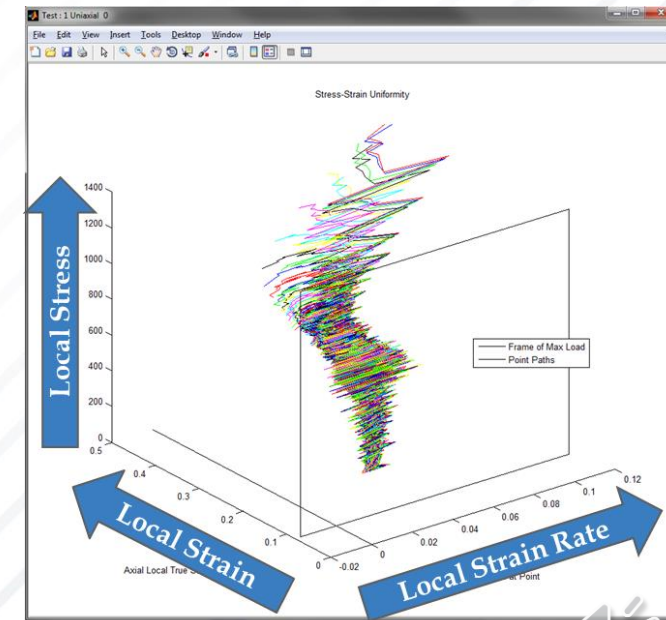


# USEFUL INFORMATION BEYOND “UE”

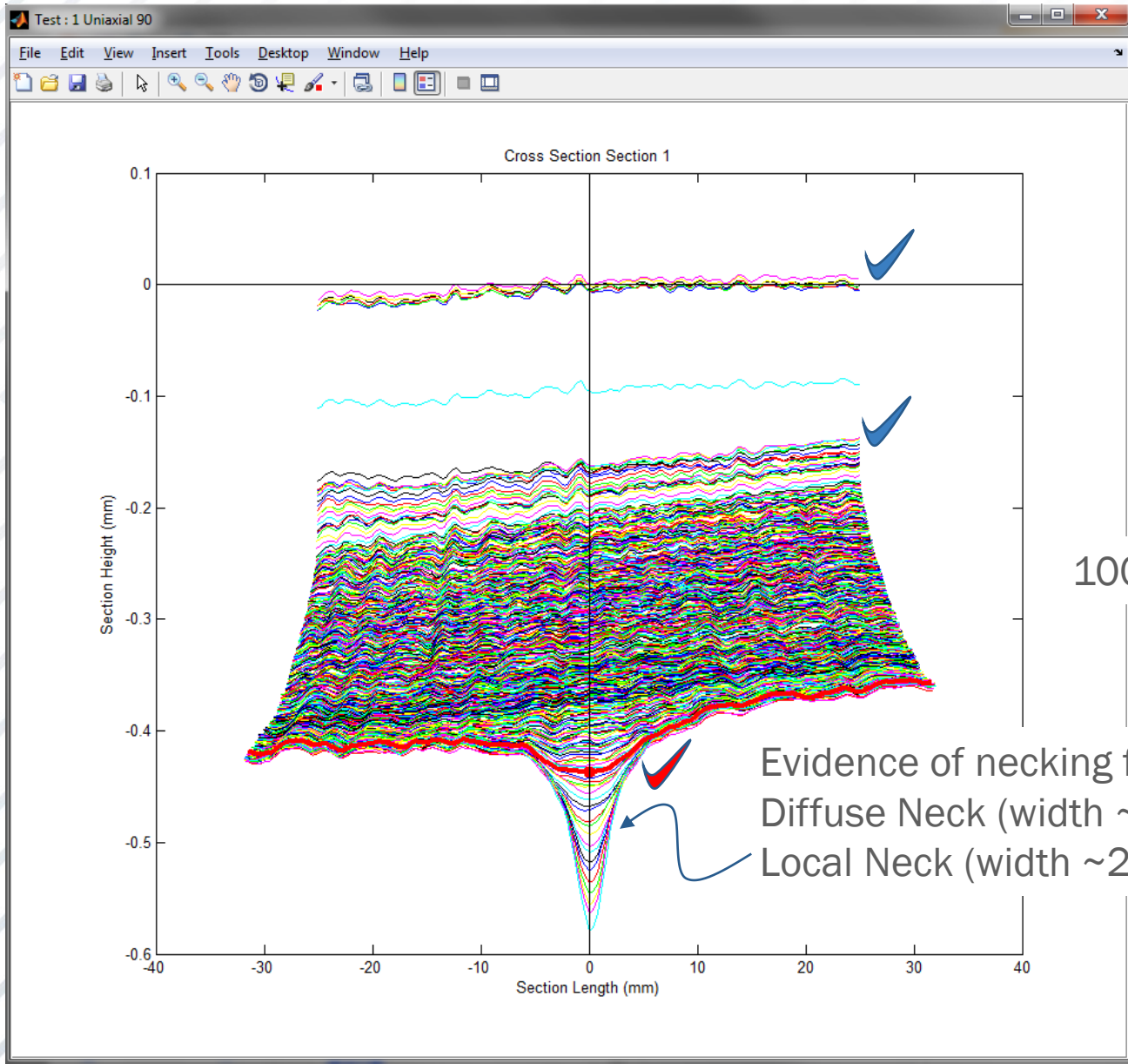


## Benefits

- 1) All 201 Points trace the 'same' hardening curve
- 2) Extends experimental curve from 8.2% engineering strain to ~61% true strain
- 3) Quantifies the degradation of the Elastic Modulus
- 4) Enables measurement of the m Value for strain rate sensitivity modeling
- 5) 'Same' hardening curve shows variation on hardening law parameters

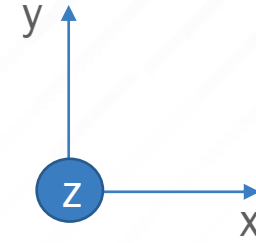


# DETECTION OF ONSET OF LOCALIZED NECKING

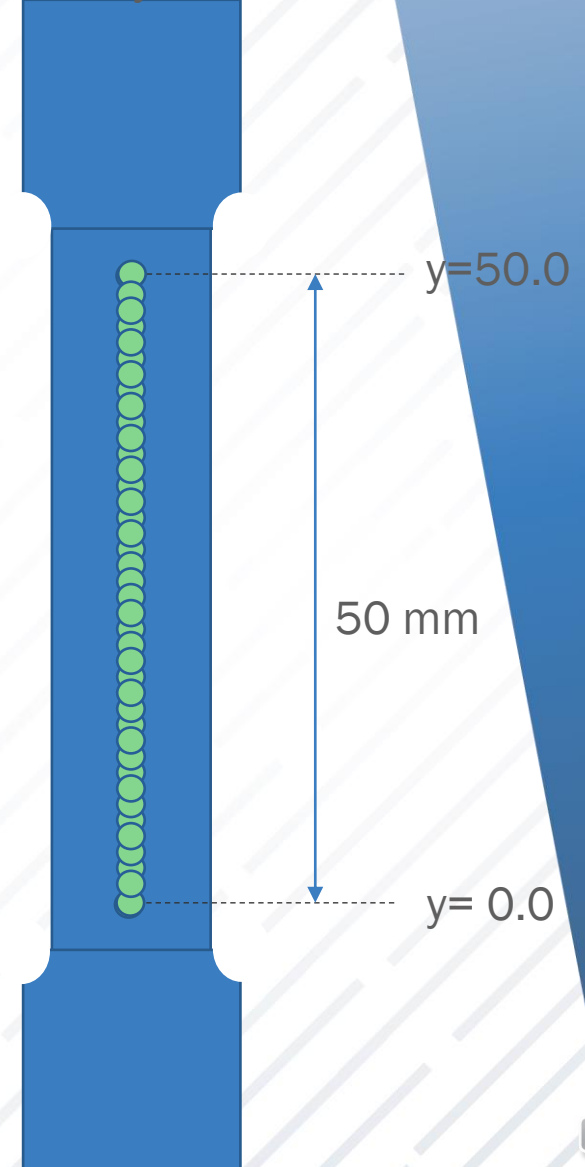


100x Magnified

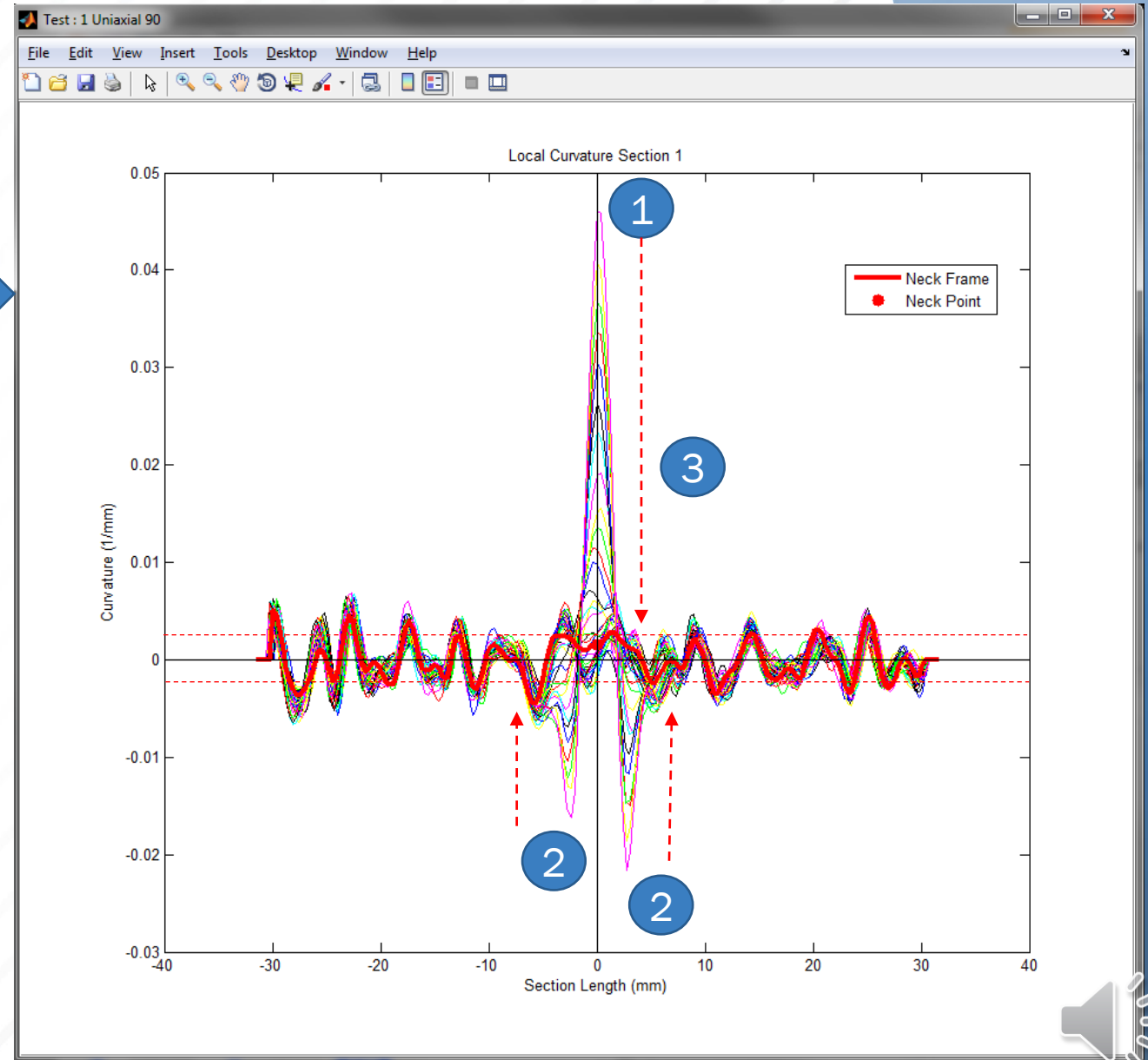
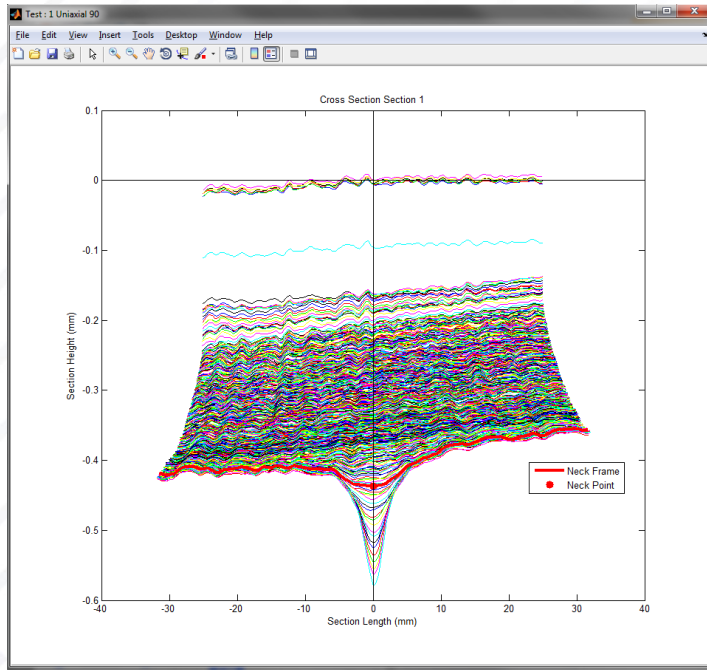
2 camera coordinate system



201 Points ●  
X, Y, Z  
Exx, Eyy, Exy  
VSG=0.5 mm



# DETECTION OF ONSET OF LOCALIZED NECKING **GDIS**



## Signature of Localized Neck

- 1) One very high positive curvature at the valley of the candidate groove in the last DIC frame.
- 2) Two high NEGATIVE peak curvatures at a location within  $2 \times$  sheet thickness of the location of the positive peak, corresponding to the two shoulders on the drop into the neck groove.
- 3) Rapid drop in the peak curvatures from frame to earlier frame to levels of curvature consistent with calculated curvatures at points outside the candidate groove (noise level).



# CURRENT APPLICATIONS OF DIC TESTING

DIC technology has been aggressively and successfully applied to

- Uniaxial Tension Tests
  - Measure R Value to High Strain
    - Average
    - Std Deviation
    - Evolution
  - Measure Hardening Law to High Strain
    - Average
    - Std Deviation
    - Strain-Rate Sensitivity
    - Young's Modulus Degradation
  - Detect Onset of Localized Necking
    - Enables accounting of Nonlinear Strain Path Effect
- Bulge Tests
- Nakajima Tests
- Marciniak Tests
- Applying to other tests...



# FUTURE

- 1) Proposal to adopt industry standard for 2 Camera DIC Data Acquisition for all ASP and Supplier/OEM material testing
  - Propose application to all 'standard' tests
  - Propose 'adaption' to all non-standard tests
- 2) Methods undergoing testing/evaluation at CAL/NIST
- 3) Propose support of a National Database based on DIC Data



# IN CLOSING...

The objective of simulation is to ELIMINATE physical testing...

Can we achieve this if we compromise  
on the definition and calibration of our Material Models?

Can we achieve this if we compromise  
on Material Testing?



# ACKNOWLEDGEMENTS

**JUNYING MIN,  
JOHN CARSLEY,  
JEONG-WHAN YOON,  
MARK IADICOLA,  
SANTE DICECCO,**

**FORMERLY GM R&D, TONGJI UNIVERSITY  
FORMERLY GM R&D, NOVELIS  
KAIST & DEAKIN UNIVERSITY  
CAL/NIST  
UNIVERSITY OF WATERLOO**



# FOR MORE INFORMATION

Thomas B. Stoughton  
General Motors Global R&D  
[thomas.b.stoughton@gm.com](mailto:thomas.b.stoughton@gm.com)





**GREAT DESIGNS IN**  
**STEEL**

**THANK YOU**

**GREAT DESIGNS IN**  
**STEEL**

**SUPPORTING INFORMATION**

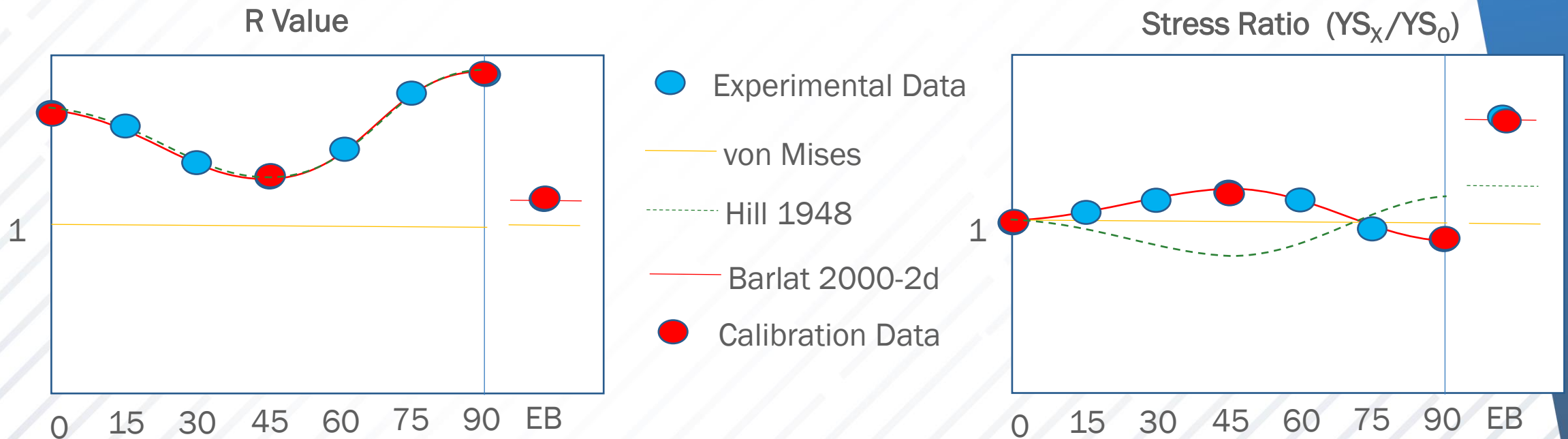
# UNIAXIAL TENSION DATA FOR SIMULATION

- 1) Young's Modulus & Poisson Ratio ←----- Isotropic handbook values
  - Anisotropy of Elasticity ←-- Typical 10-20% variation affects spring-back proportionally
  - Degradation of YM with strain ←----- Requires load/unload/reload test
- 2) Proportional Limit (Elastic-to-Plastic Transition) ←-- 0.2% Offset Yield Stress
- 3) Hardening Law (True Stress vs Plastic Strain) ←----- YS, UTS, UE → K, n, e0
  - Extension beyond max load ←-- Needed if expecting to predict conditions up to fracture
  - Kinematic Hardening ←----- Requires tension-compression test
  - Anisotropic Hardening ←----- Requires tests in at least 3 loading orientations
  - Strain rate effects ←----- Requires jump test or multiple tests
- 4) R Value (Ratio of Plastic Strain Rates) ←----- based on Total NET Strain
- 5) Onset of Localized Necking ←----- Not detectable
- 6) Local Fracture Strain ←----- Not measured

# HISTORY OF CONSTITUTIVE MODELS

The ultimate objective of simulation is to ELIMINATE physical testing...

Can we achieve this if we compromise on the definition and calibration of our Material Models?



# TRADITIONAL UNIAXIAL TENSION TEST

## Standard Results

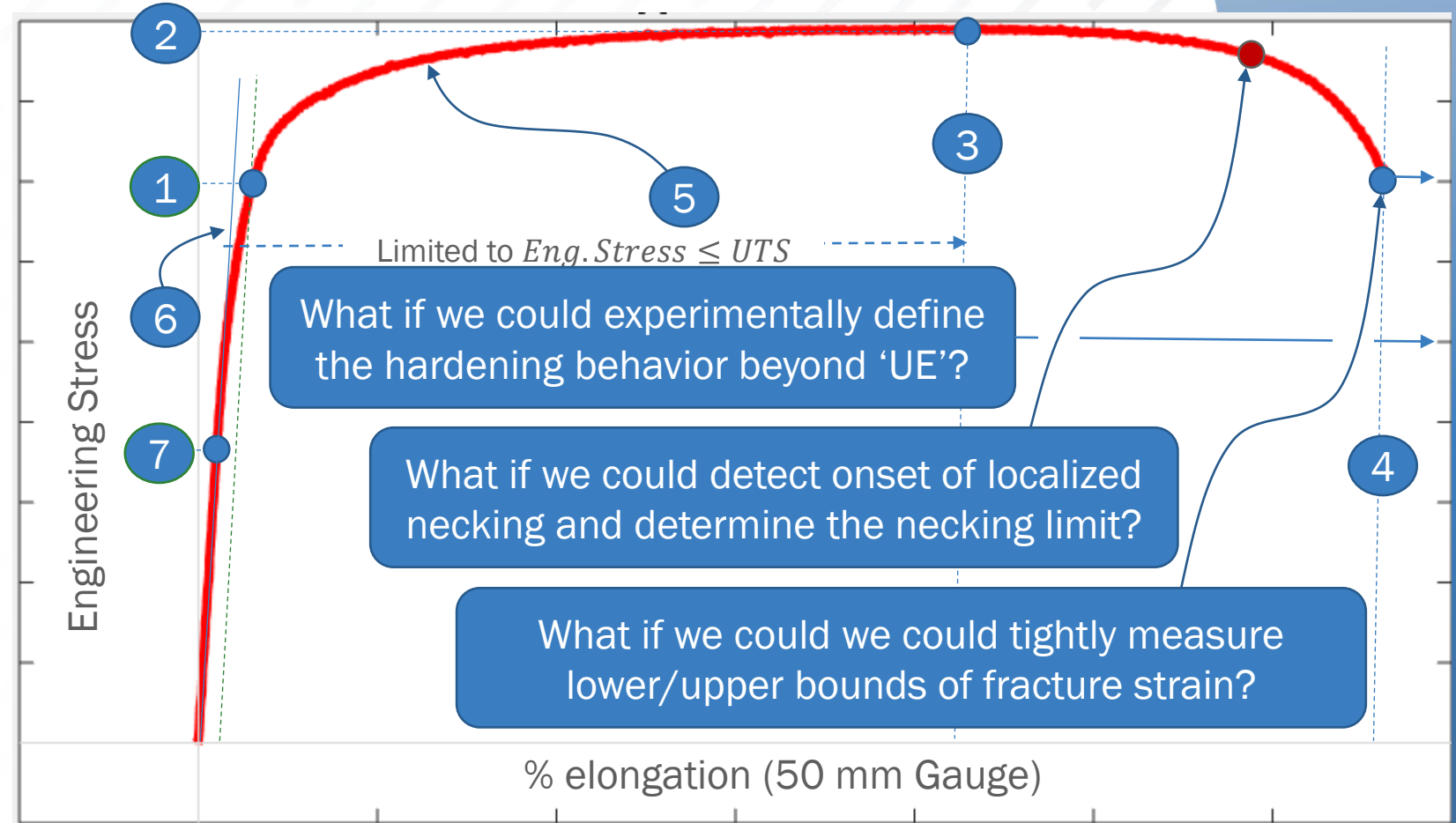
- 1) 0.2% Offset Yield Stress
- 2) Ultimate Tensile Strength
- 3) Uniform Elongation
- 4) Total Elongation
- 5) Hardening Behavior
- 6) Elastic Modulus
- 7) Proportional Limit

## Add a Width Strain Gauge

- 8) R Value
- 9) Poisson Ratio

## Additional Needs

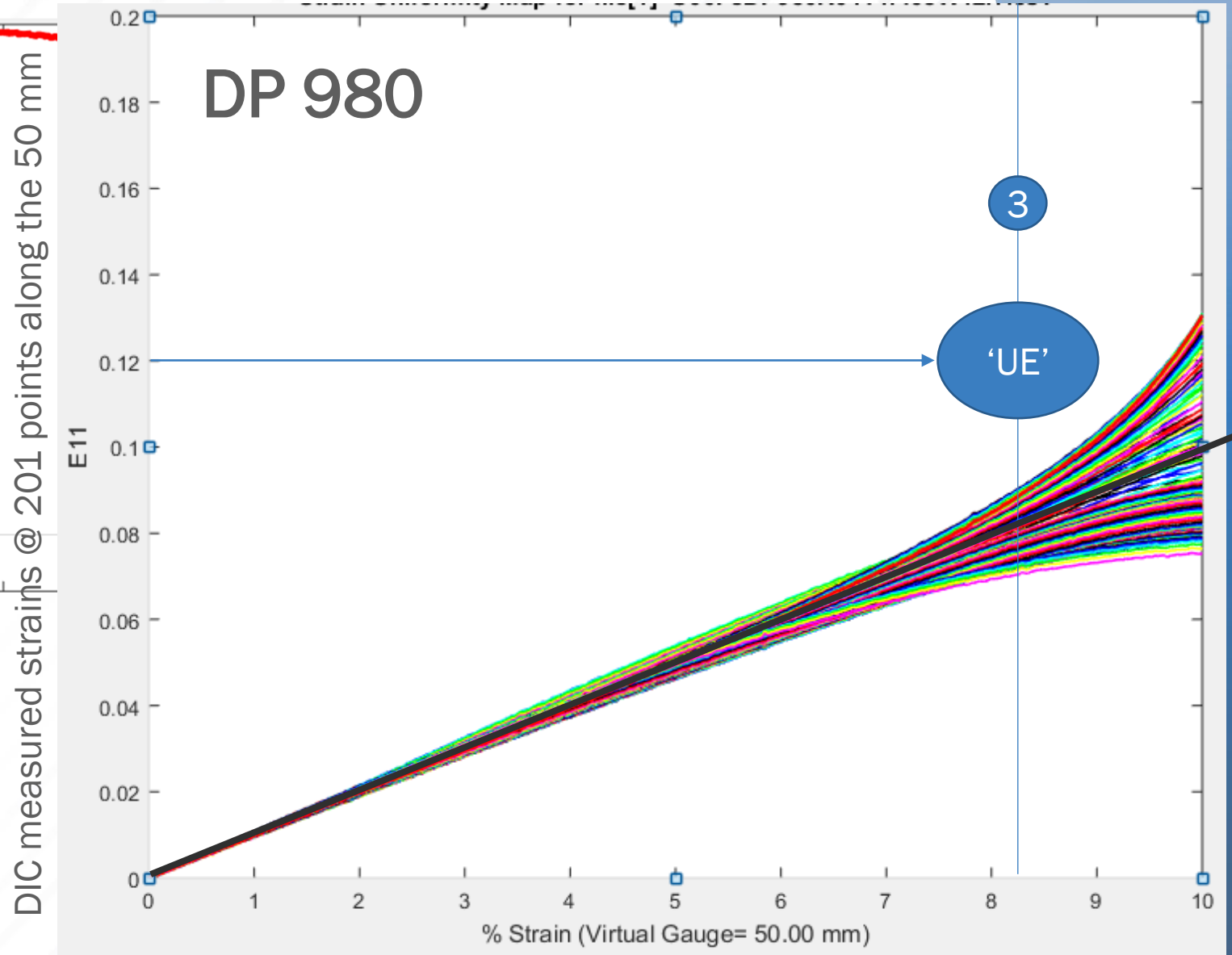
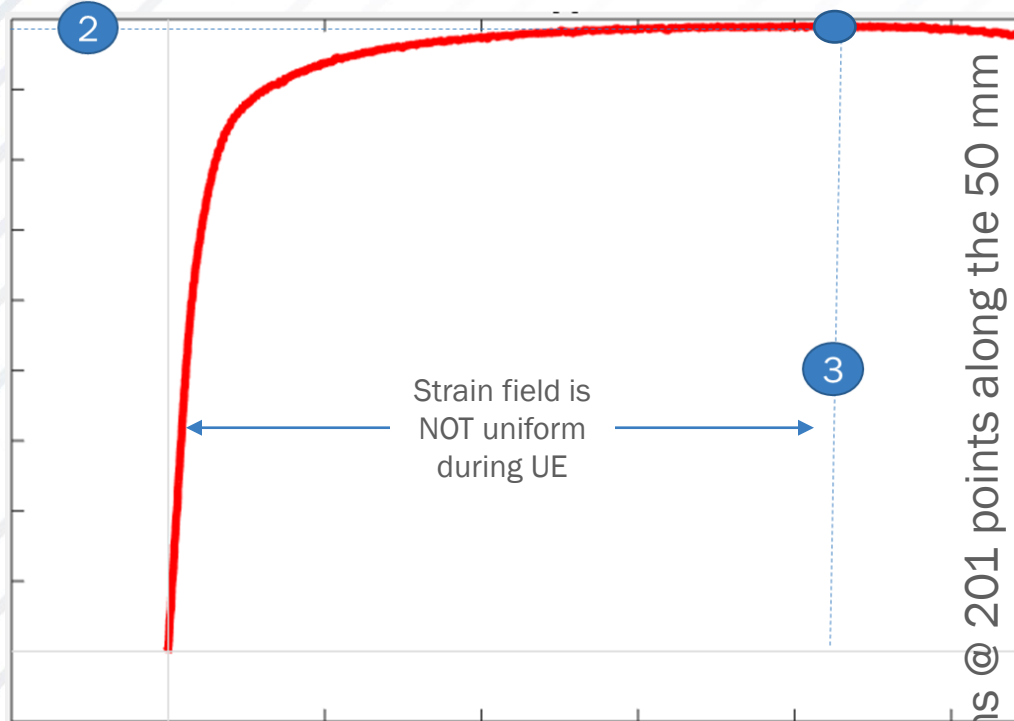
- 10) m Value (jump tests)
- 11) YM degradation (load/unload)
- 12) Property variation (repeats)



Additional Tension Tests

What if we could get a handle on this from a SINGLE Uniaxial Tension Test?

# IS UNIFORM ELONGATION UNIFORM?



DIC Analysis  
Clearly Shows  
the Answer is NO

% Stretch of end points of a 50 mm Gauge

# EXAMPLE OF CSV FILE CONTENT

	A	B	C	D	E	F
1	X [mm]	Y [mm]	Z [mm]	exx [1] - Hencky	eyy [1] - Hencky	exy [1] - Hencky
2	0.000	-25.000	0.019	0.00000	0.00000	0.00000
3	0.000	-25.001	0.018	-0.00009	-0.00002	-0.00009
4	-0.001	-25.000	0.020	-0.00002	0.00011	-0.00012
5	0.001	-24.998	0.019	0.00004	-0.00012	-0.00007
6	0.000	-24.999	0.017	-0.00026	-0.00020	-0.00011
7	0.000	-25.001	0.016	-0.00002	0.00000	-0.00004
8	0.000	-24.998	0.018	-0.00011	-0.00023	-0.00001
9	0.000	-25.000	0.019	0.00002	0.00002	-0.00006
10	0.000	-25.008	0.016	-0.00007	0.00003	-0.00004
11	0.001	-25.014	0.013	-0.00009	0.00015	-0.00017
12	0.000	-25.018	0.012	-0.00014	0.00021	-0.00010

1<sup>st</sup> of 201 Points...

580	-0.06749	-31.9836	-0.04415	-0.0332459	0.0786817	-0.000278133
581	-0.06814	-31.9976	-0.04339	-0.0331969	0.0786263	-0.000335343
582	-0.07185	-32.0133	-0.04352	-0.0330825	0.0786386	-0.000235271
583	-0.07418	-32.0291	-0.03997	-0.0333873	0.0785958	-0.00036776
584	-0.07513	-32.0416	-0.04367	-0.033368	0.0784631	-0.000312553
585	-0.07954	-32.0598	-0.0395	-0.0332215	0.0783598	-0.000227205
586	-0.08045	-32.0748	-0.04288	-0.0331713	0.0782322	-0.000263781
587	-0.08527	-32.0915	-0.0449	-0.0333184	0.0784897	-0.000232748
588	-0.0849	-32.1053	-0.04264	-0.0331525	0.0783864	-0.000361529
589	-0.0867	-32.1204	-0.0467	-0.0330774	0.0782752	-0.000255177
590	-0.0921	-32.1386	-0.04722	-0.0331462	0.0782398	-0.000279237
591						

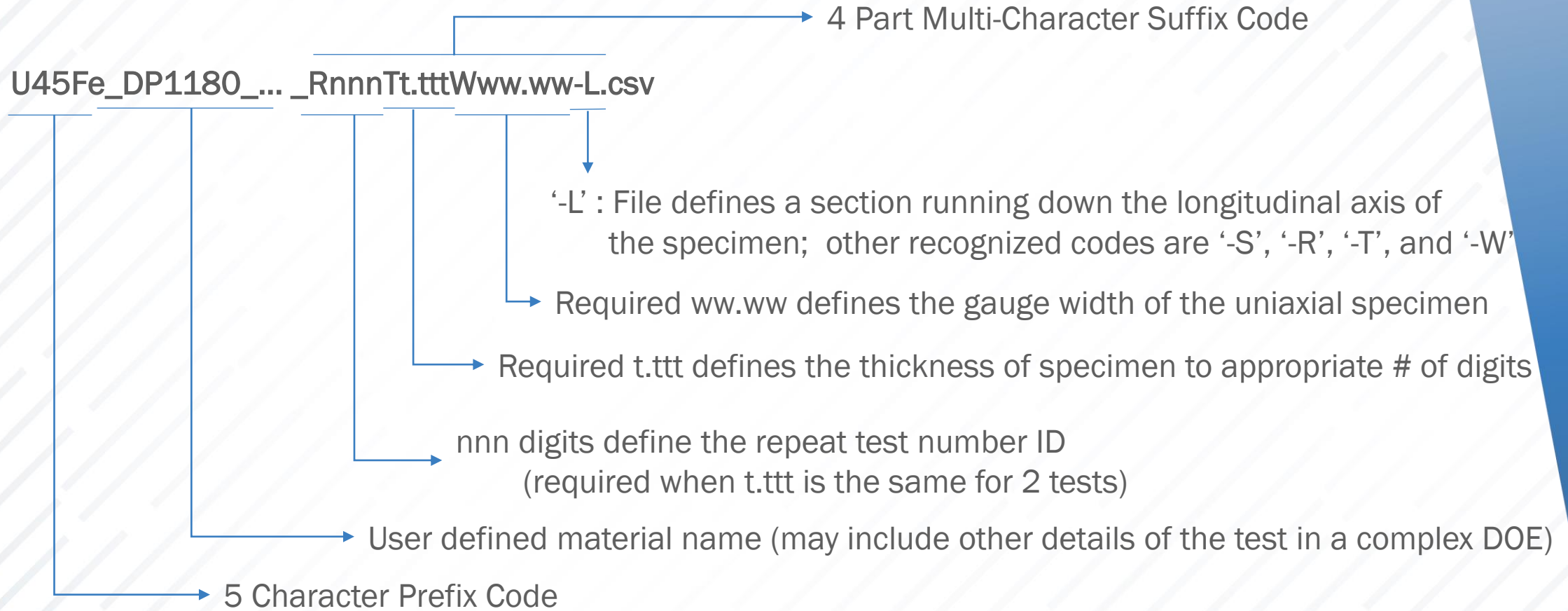
U00FeDP980\_R01T1.405W12.70-L

ATJ	ATK	ATL	ATM	ATN	ATO	ATP	ATQ	ATR	ATS
- Hen	Count	Time_1	Time_0	Dev2/ai0	Dev2/ai1	Dev2/ai2	Dev2/ai3	acement	Force_(kN)
75E-18	10	132.85	132.85	-2.536	0.0033	-0.0003	0.0004	-25.3598	0.033
00013	41	148.35	148.35	-2.535	0.0013	0.0004	-0.0006	-25.35	0.013
00012	42	148.85	148.85	-2.5353	-0.0009	-0.0006	-0.0013	-25.3533	-0.009
76E-05	43	149.35	149.35	-2.536	0.0017	-0.0003	-0.0013	-25.3598	0.017
00025	44	149.85	149.85	-2.5344	0.0072	0.0004	-0.0009	-25.3435	0.072
70E-05	45	150.35	150.35	-2.5334	0.0072	0	-0.0006	-25.3338	0.072
79E-05	46	150.85	150.85	-2.5347	-0.0019	-0.0003	-0.0003	-25.3468	-0.019
00013	47	151.35	151.35	-2.5344	0.0056	0	-0.0006	-25.3435	0.056
00018	48	151.85	151.85	-2.5334	0.0377	0	0	-25.3338	0.377
00014	49	152.60	152.60	-2.5334	0.0611	-0.0013	0.0004	-25.3338	0.611
00014	50	153.10	153.10	-2.5321	0.0883	-0.0006	0	-25.3208	0.883

Time, Load, Misc. Data

00024	618	673.20	673.20	-1.7913	1.5589	-0.0019	0.0007	-17.9127	15.589
00022	619	674.20	674.20	-1.7887	1.545	-0.0013	-0.0006	-17.8868	15.450
00028	620	675.20	675.20	-1.7877	1.5326	0.0004	-0.0003	-17.877	15.326
00028	621	676.20	676.20	-1.7861	1.5307	-0.0013	-0.0009	-17.8608	15.307
00003	622	677.20	677.20	-1.7854	1.5096	-0.0003	-0.0003	-17.8543	15.096
00022	623	678.20	678.20	-1.7841	1.5083	-0.0006	0.0007	-17.8413	15.083
00026	624	679.20	679.20	-1.7822	1.4869	-0.0003	-0.0016	-17.8218	14.869
00002	625	680.20	680.20	-1.7812	1.4781	-0.0009	0	-17.8121	14.781
7E-05	626	681.20	681.20	-1.7789	1.4645	-0.0009	-0.0013	-17.7894	14.645
00026	627	682.20	682.20	-1.7783	1.444	0.0004	-0.0003	-17.7829	14.440
00034	628	683.20	683.20	-1.7763	1.4349	-0.0003	-0.0009	-17.7634	14.349

# PROPOSED DIC FILE NAMING CONVENTION



1<sup>st</sup> Character : BUMNVCS Code : Bulge, Uniaxial, Marciniak, Nakajima, V-Bend, Cruciform, Shear  
Character 2&3 : Two-digit angle of Major Loading Axis to the RD of the sheet  
Character 4&5 : Chemical code of Primary Element (Fe, AL, or Mg)  
(used to initialize elastic properties to improve automation of the elastic fitting)